High Speed Communication Circuits and Systems
Lecture 4
Generalized Reflection Coefficient, Smith Chart, Integrated Passive Components

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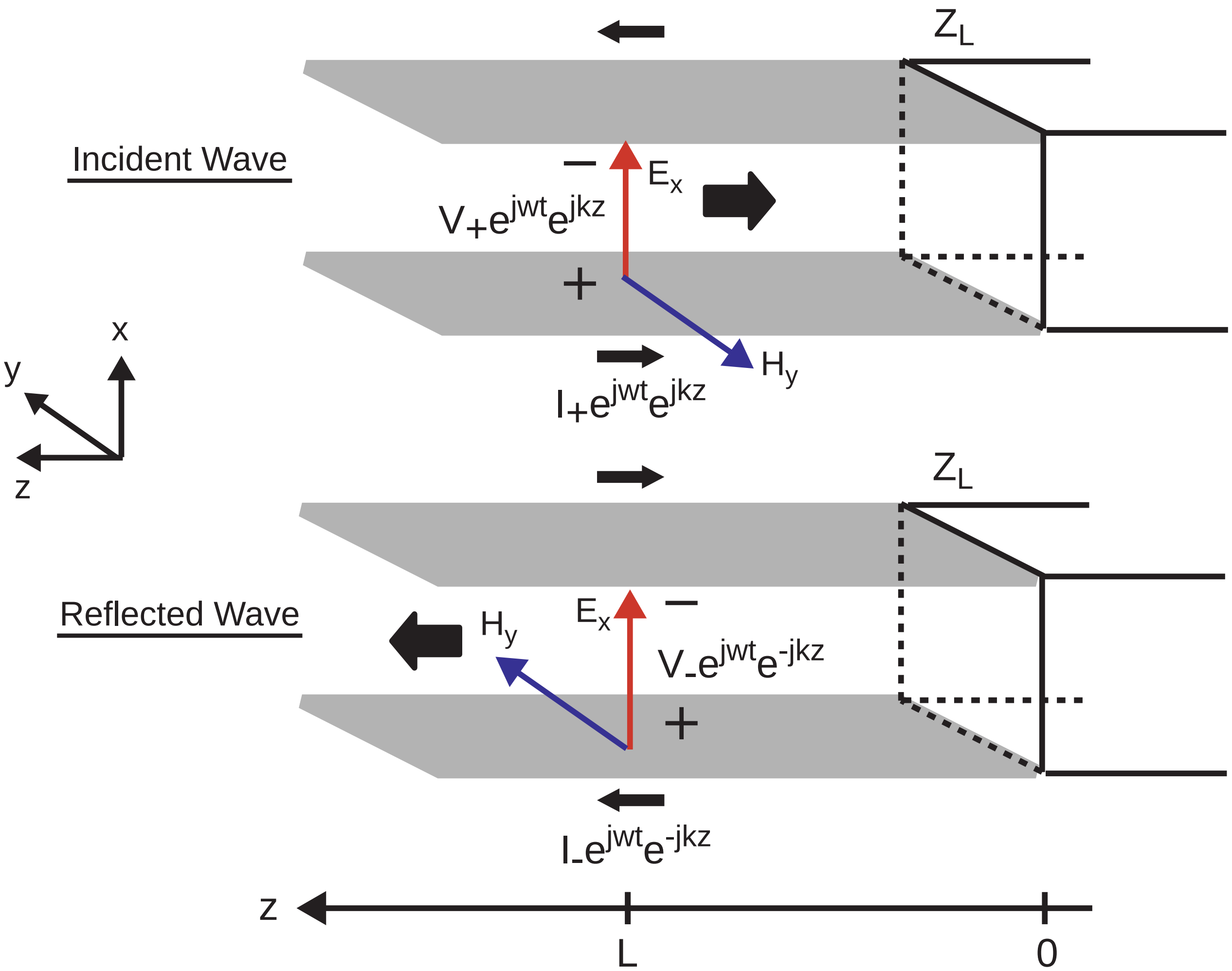
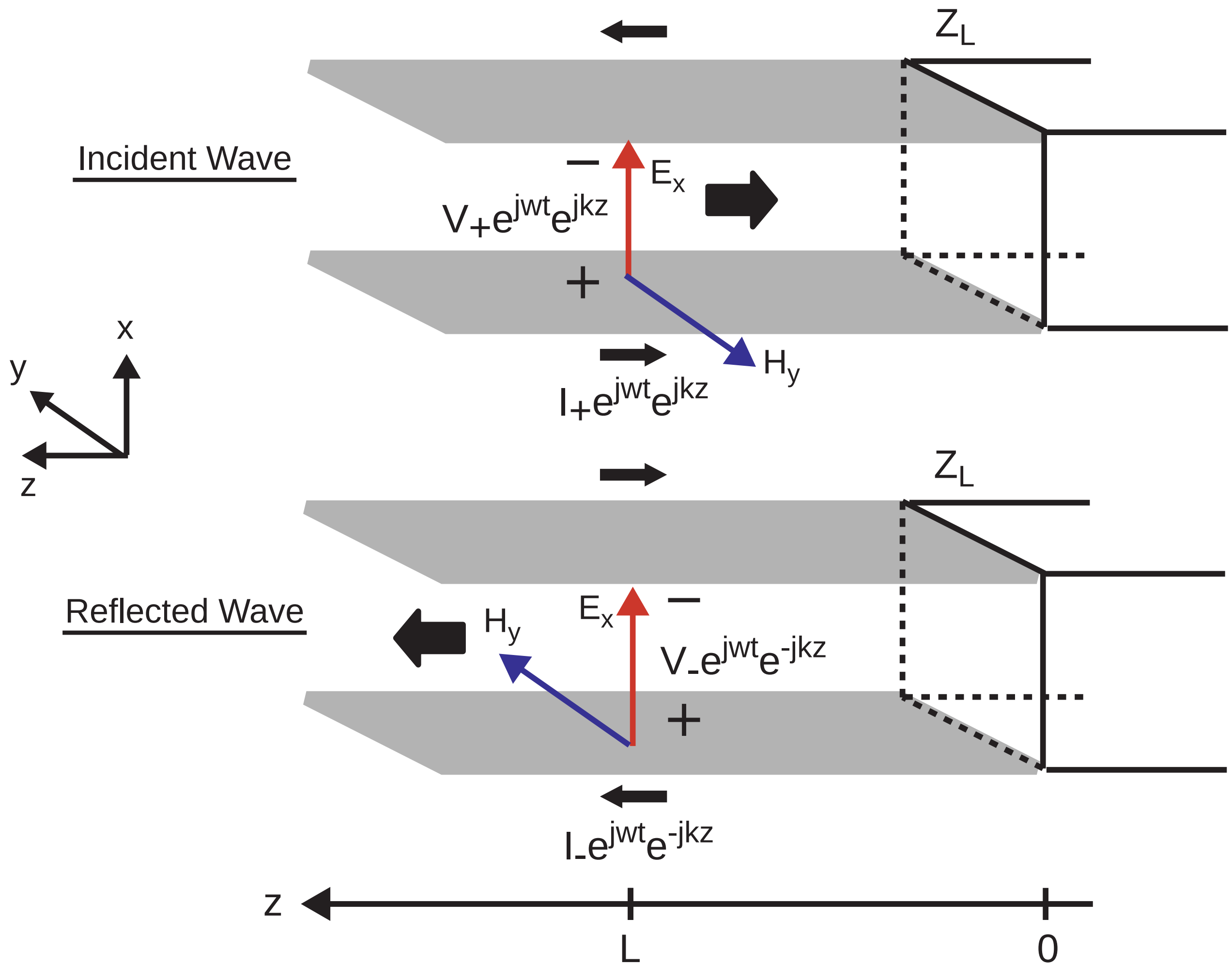
Determine Voltage and Current At Different Positions



- **Incident and reflected waves must be added together**

Determine Voltage and Current At Different Positions



$$V(z,t) = V_+ e^{jwt} e^{jkz} + V_- e^{jwt} e^{-jkz}$$
$$I(z,t) = I_+ e^{jwt} e^{jkz} - I_- e^{jwt} e^{-jkz}$$

Define Generalized Reflection Coefficient

$$V(z,t) = V_+ e^{jwt} e^{jkz} + V_- e^{jwt} e^{-jkz}$$

$$I(z,t) = I_+ e^{jwt} e^{jkz} - I_- e^{jwt} e^{-jkz}$$

$$V(z,t) = V_+ e^{jwt} e^{jkz} \left(1 + \frac{V_-}{V_+} e^{-2jkz}\right)$$

$$\Downarrow$$

$$V(z,t) = V_+ e^{jwt} e^{jkz} \left(1 + \Gamma_L e^{-2jkz}\right)$$

$$\Downarrow$$

$$V(z,t) = V_+ e^{jwt} e^{jkz} \left(1 + \Gamma(z)\right)$$

Similarly: $$I(z,t) = I_+ e^{jwt} e^{jkz} \left(1 - \Gamma(z)\right)$$

$$\Rightarrow \quad \Gamma(z) = \Gamma_L e^{-2jkz}$$

A Closer Look at Γ(z)

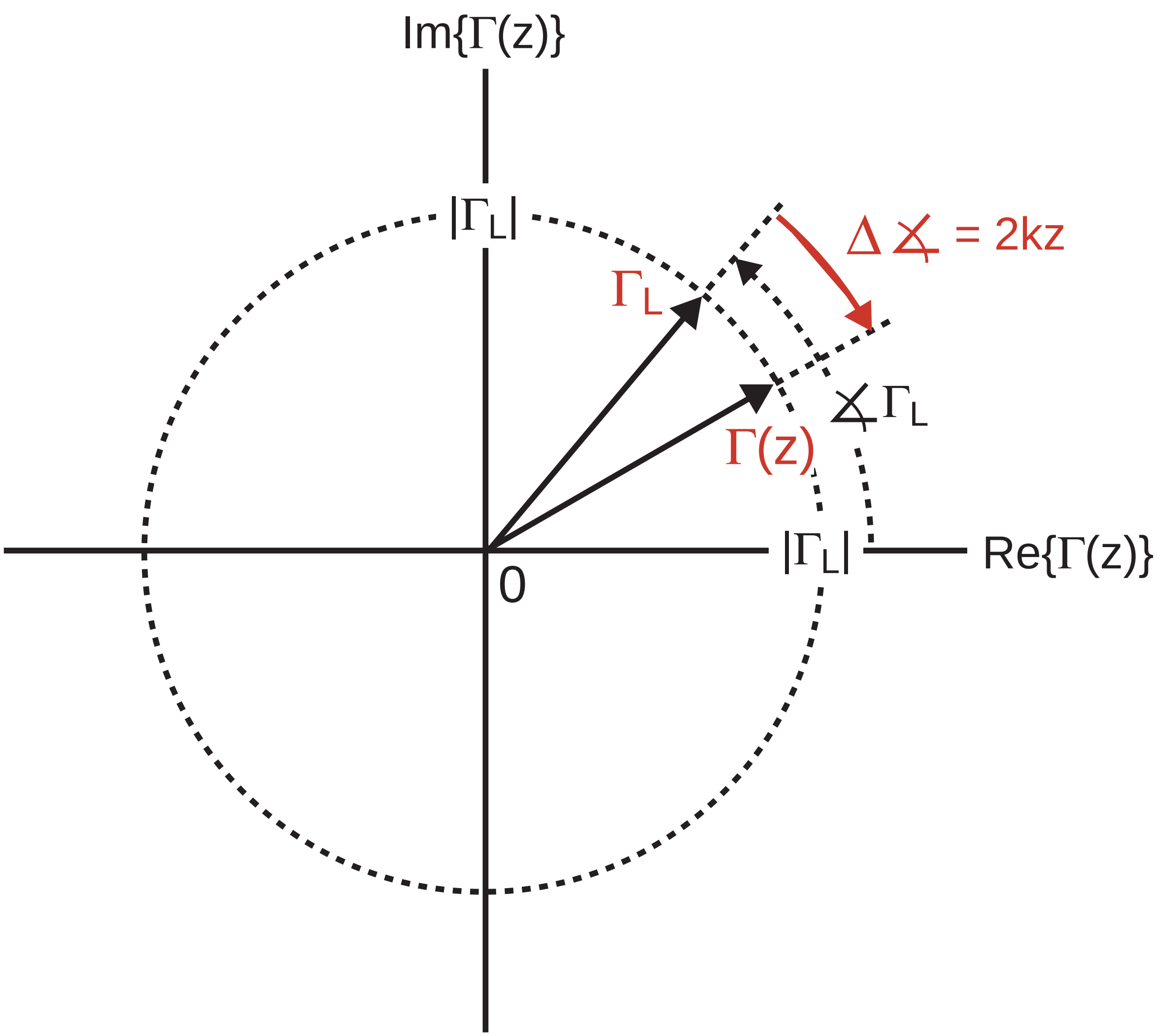
- **Recall Γ_L is**

$$\Gamma_L = \frac{Z_L - Z_o}{Z_L + Z_o}$$

Note: $|\Gamma_L| \leq 1$

for $Re\{Z_L/Z_o\} \geq 0$

$$\Gamma(z) = \Gamma_L e^{-2jkz}$$



- **We can view Γ(z) as a complex number that rotates clockwise as z (distance from the load) increases**

Calculate $|V_{max}|$ and $|V_{min}|$ Across The Transmission Line

- **We found that**

$$V(z,t) = V_+ e^{jwt} e^{jkz} (1 + \Gamma(z))$$

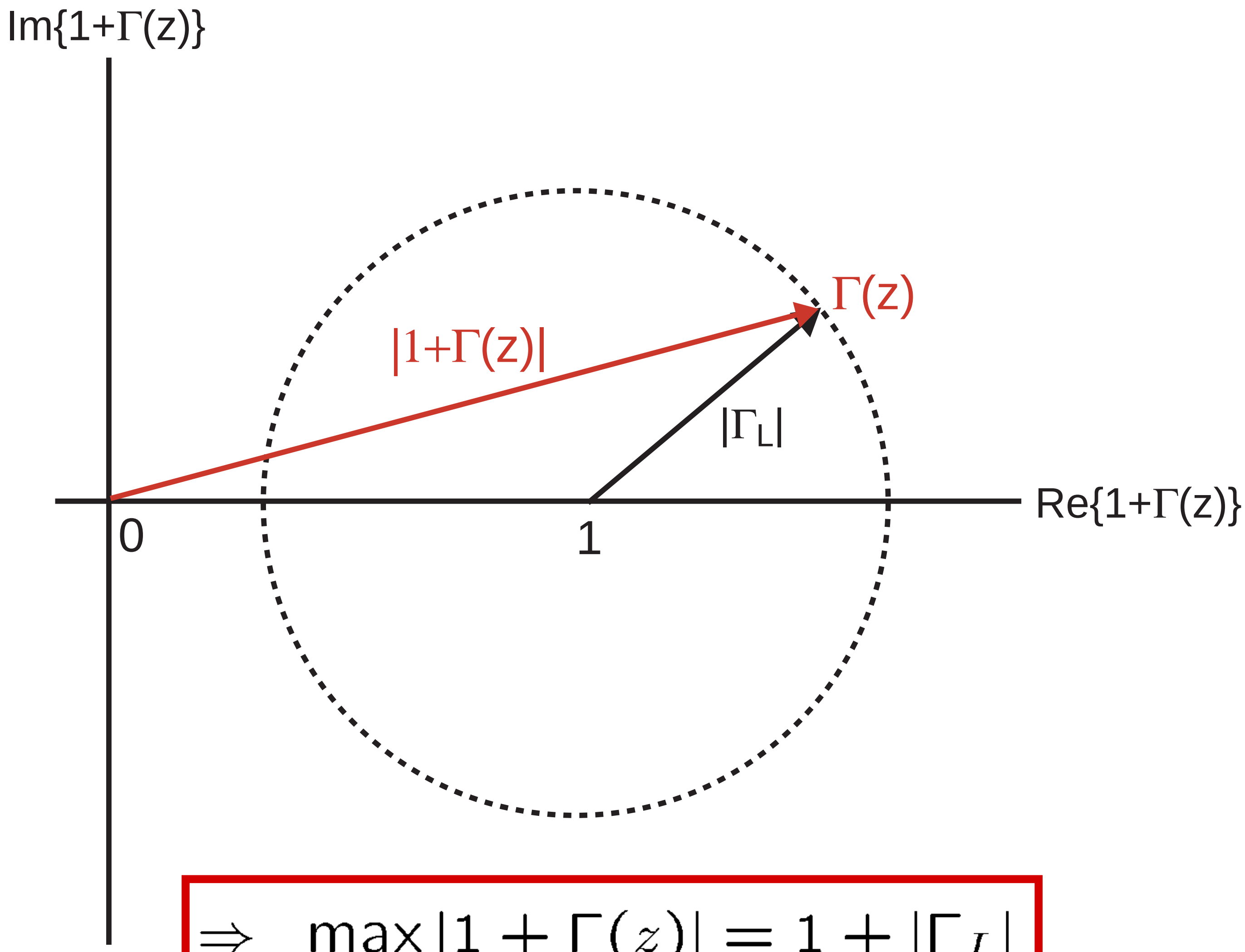
- **So that the max and min of V(z,t) are calculated as**

$$\Rightarrow \quad V_{max} = \max |V(z,t)| = |V_+| \max |1 + \Gamma(z)|$$

$$\Rightarrow \quad V_{min} = \min |V(z,t)| = |V_+| \min |1 + \Gamma(z)|$$

- **We can calculate this geometrically!**

A Geometric View of $|1 + \Gamma(z)|$

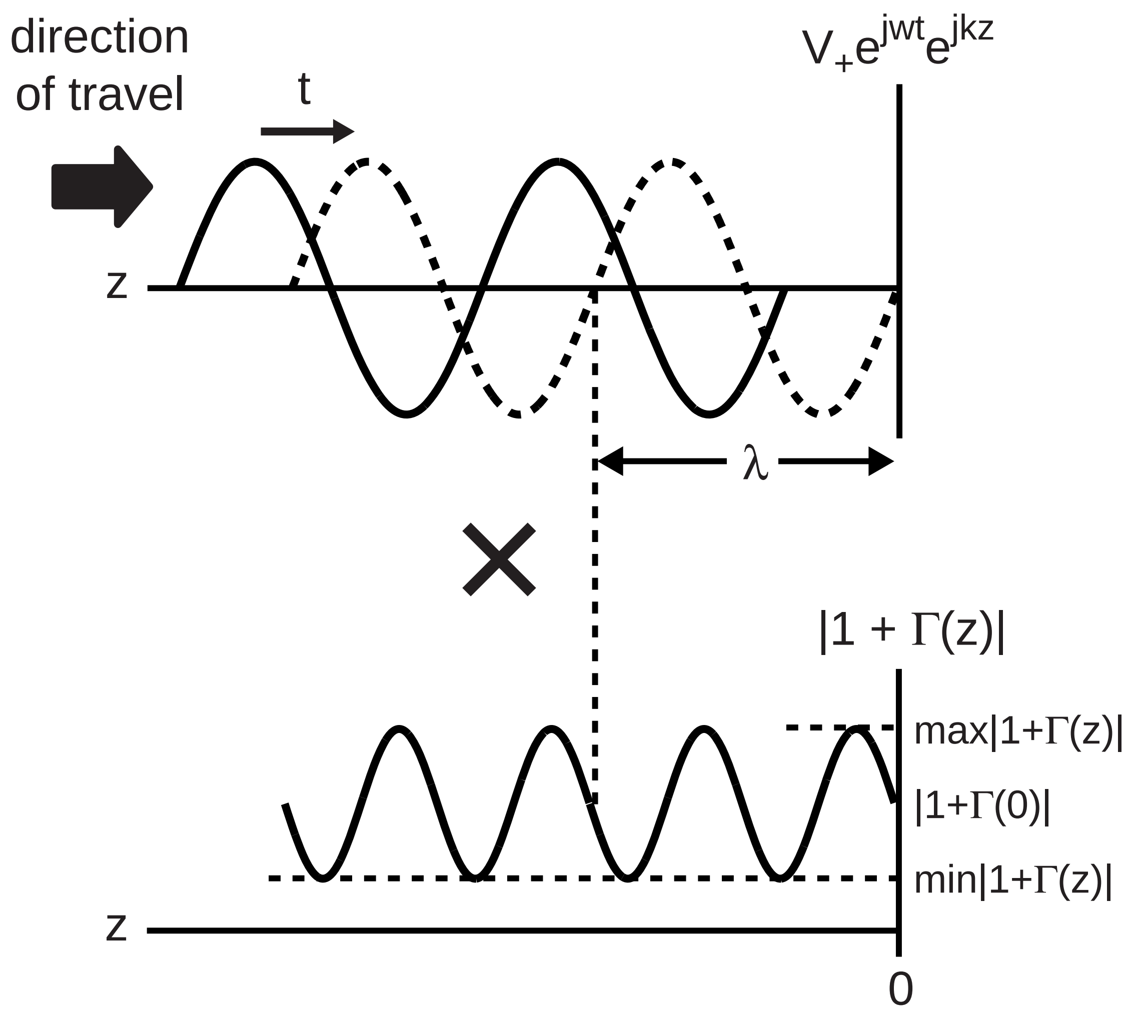


$$\Rightarrow \quad \max|1+\Gamma(z)| = 1 + |\Gamma_L|$$

$$\Rightarrow \quad \min|1+\Gamma(z)| = 1 - |\Gamma_L|$$

Reflections Cause Amplitude to Vary Across Line

- **Equation:** $V(z,t) = V_+ e^{jwt} e^{jkz} \left|1 + \Gamma(z)\right| e^{j\angle(1+\Gamma(z))}$
- **Graphical representation:**



Voltage Standing Wave Ratio (VSWR)

- **Definition**

$$\text{VSWR} = \frac{V_{max}}{V_{min}} = \frac{|V_+|(1+|\Gamma_L|)}{|V_+|(1-|\Gamma_L|)} = \frac{1+|\Gamma_L|}{1-|\Gamma_L|}$$

- **For passive load (and line)**

$$|\Gamma_L| \leq 1 \quad \Rightarrow \quad 1 \leq \text{VSWR} \leq \infty$$

$$\underset{|\Gamma_L| = 0}{\uparrow} \qquad\qquad \underset{|\Gamma_L| = 1}{\uparrow}$$

- **We can infer the magnitude of the reflection coefficient based on VSWR**

$$|\Gamma_L| = \frac{\text{VSWR}-1}{\text{VSWR}+1}$$

Reflections Influence Impedance Across The Line

- **From Slide 4**

$$V(z,t) = V_+ e^{jwt} e^{jkz} (1 + \Gamma(z))$$

$$I(z,t) = I_+ e^{jwt} e^{jkz} (1 - \Gamma(z))$$

$$\Rightarrow \quad Z(z,t) = \frac{V_+(1+\Gamma(z))}{I_+(1-\Gamma(z))} = Z_o \frac{1+\Gamma(z)}{1-\Gamma(z)}$$

  - **Note: not a function of time! (only of distance from load)**

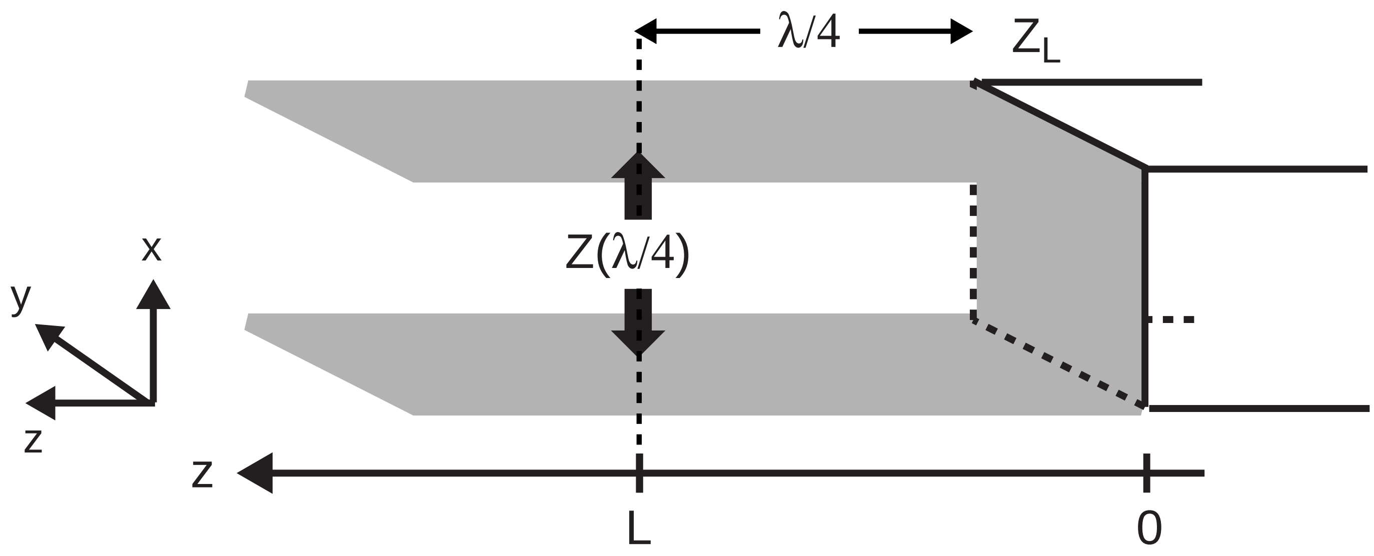
- **Alternatively**

$$Z(z) = Z_o \frac{1+\Gamma_L e^{-2jkz}}{1-\Gamma_L e^{-2jkz}}$$

  - **From Lecture 2:** $\lambda = \frac{T}{\sqrt{\mu\epsilon}} = \frac{wT}{w\sqrt{\mu\epsilon}} = \frac{2\pi f T}{k} = \frac{2\pi}{k}$

$$Z(z) = Z_o \frac{1+\Gamma_L e^{-j(4\pi/\lambda)z}}{1-\Gamma_L e^{-j(4\pi/\lambda)z}}$$

Example: $Z(\lambda/4)$ with Shorted Load



- **Calculate reflection coefficient**

$$\Gamma_L = \frac{Z_L - Z_o}{Z_L + Z_o} = \frac{0 - Z_o}{0 + Z_o} = -1$$

- **Calculate generalized reflection coefficient**

$$\Gamma(\lambda/4) = \Gamma_L e^{-j(4\pi/\lambda)(\lambda/4)} = \Gamma_L e^{-j\pi} = -\Gamma_L = 1$$

- **Calculate impedance**

$$Z(\lambda/4) = Z_o \frac{1 + \Gamma(z)}{1 - \Gamma(z)} = \infty \; !$$

Generalize Relationship Between Z(λ/4) and Z(0)

- **General formulation**

$$Z(z) = Z_o \frac{1 + \Gamma_L e^{-j(4\pi/\lambda)z}}{1 - \Gamma_L e^{-j(4\pi/\lambda)z}}$$

- **At load (z=0)**

$$Z_L = Z(0) = Z_o \frac{1 + \Gamma_L}{1 - \Gamma_L}$$

- **At quarter wavelength away (z = λ/4)**

$$Z(\lambda/4) = Z_o \frac{1 - \Gamma_L}{1 + \Gamma_L} = \frac{Z_o^2}{Z_L}$$

  - **Impedance is inverted!**
    - Shorts turn into opens
    - Capacitors turn into inductors

Now Look At $Z(\Delta)$ (Impedance Close to Load)

- **Impedance formula (Δ very small)**

$$Z(\Delta) = Z_o \frac{1 + \Gamma_L e^{-2jk\Delta}}{1 - \Gamma_L e^{-2jk\Delta}}$$

  - **A useful approximation:** $e^{-jx} \approx 1 - jx \;\; \text{for } x \ll 1$

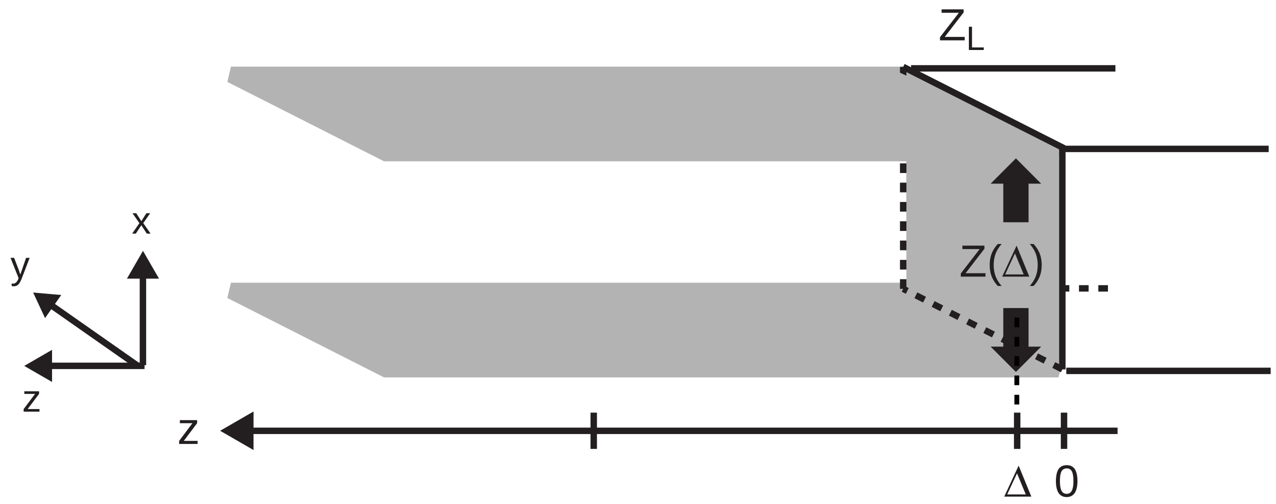
$$\Rightarrow \;\; e^{-2jk\Delta} \approx 1 - 2jk\Delta$$

  - **Recall from Lecture 2:** $k = w\sqrt{LC}, \quad Z_o = \sqrt{\frac{L}{C}}$

- **Overall approximation:**

$$Z(\Delta) \approx \left(\sqrt{\frac{L}{C}}\right) \frac{1 + \Gamma_L(1 - 2jw\sqrt{LC}\Delta)}{1 - \Gamma_L(1 - 2jw\sqrt{LC}\Delta)}$$

Example: Look At $Z(\Delta)$ With Load Shorted

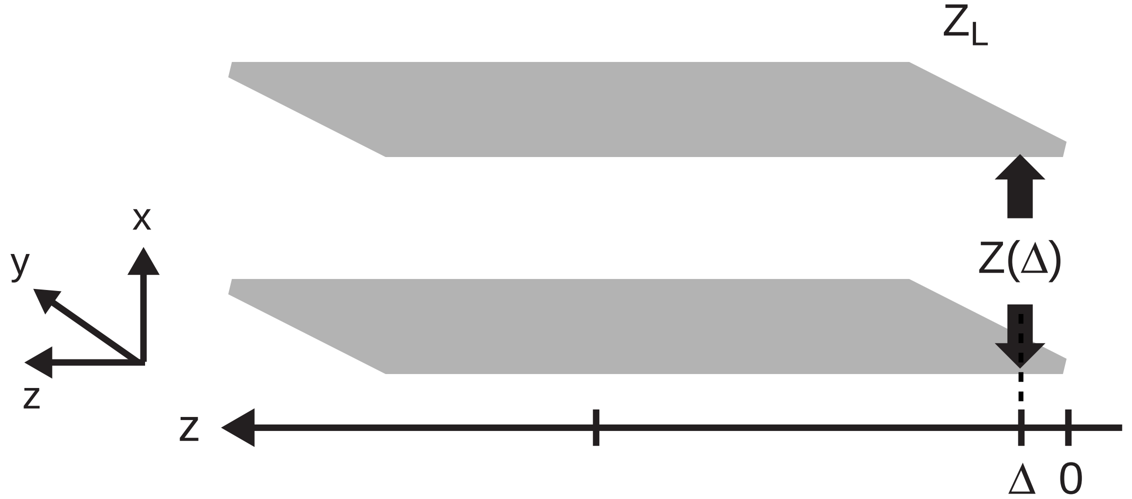


$$Z(\Delta) \approx \left(\sqrt{\frac{L}{C}}\right) \frac{1 + \Gamma_L(1 - 2jw\sqrt{LC}\Delta)}{1 - \Gamma_L(1 - 2jw\sqrt{LC}\Delta)}$$

- **Reflection coefficient:** $$\Gamma_L = \frac{Z_L - Z_o}{Z_L + Z_o} = \frac{0 - Z_o}{0 + Z_o} = -1$$
- **Resulting impedance looks inductive!**

$$Z(\Delta) \approx \left(\sqrt{\frac{L}{C}}\right) \frac{1 - (1 - 2jw\sqrt{LC}\Delta)}{1 + (1 - 2jw\sqrt{LC}\Delta)} \approx jwL\Delta$$

Example: Look At Z(Δ) With Load Open

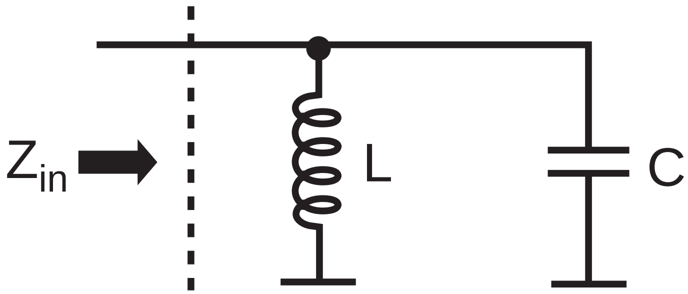


$$Z(\Delta) \approx \left(\sqrt{\frac{L}{C}}\right)\frac{1+\Gamma_L(1-2jw\sqrt{LC}\Delta)}{1-\Gamma_L(1-2jw\sqrt{LC}\Delta)}$$

- **Reflection coefficient:** $$\Gamma_L = \frac{Z_L - Z_o}{Z_L + Z_o} = \frac{\infty - Z_o}{\infty + Z_o} = 1$$
- **Resulting impedance looks capacitive!**

$$Z(\Delta) \approx \left(\sqrt{\frac{L}{C}}\right)\frac{1+(1-2jw\sqrt{LC}\Delta)}{1-(1-2jw\sqrt{LC}\Delta)} \approx \frac{1}{jwC\Delta}$$

Consider an Ideal LC Tank Circuit



$$Z_{in}(w) = \frac{1}{jwC} || jwL = \frac{jwL}{1 - w^2LC}$$

- **Calculate input impedance about resonance**

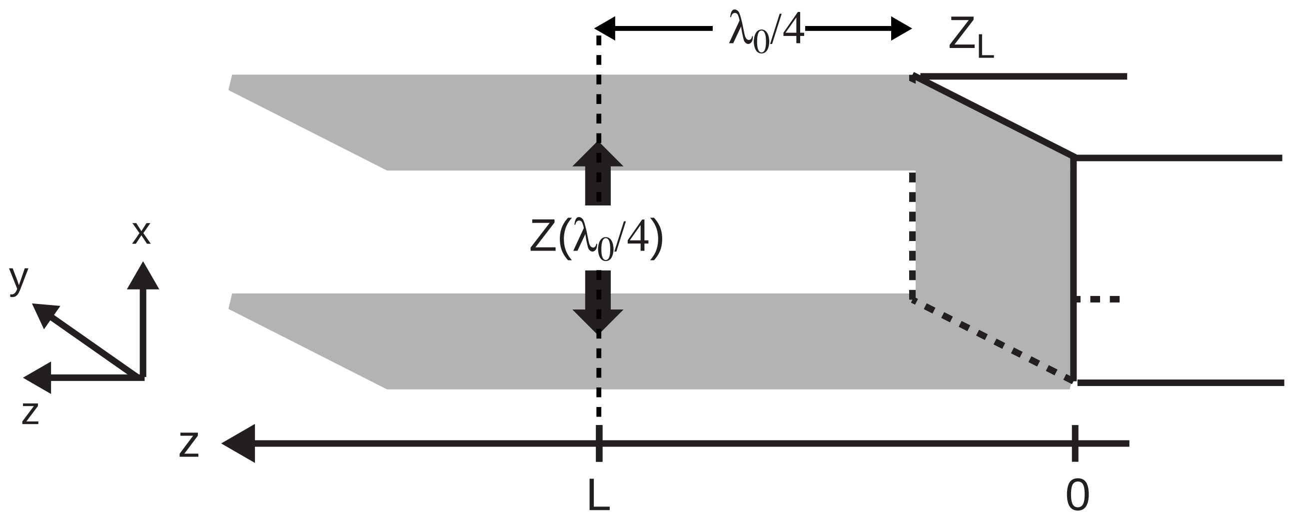
$$\text{Consider } w = w_o + \Delta w, \text{ where } w_o = \frac{1}{\sqrt{LC}}$$

$$Z_{in}(\Delta w) = \frac{j(w_o + \Delta w)L}{1 - (w_o + \Delta w)^2 LC}$$

$$= \frac{j(w_o + \Delta w)L}{\underbrace{1 - w_o^2 LC}_{= 0} - 2\Delta w(w_o LC) - \underbrace{\Delta w^2 LC}_{\text{negligible}}}$$

$$\Rightarrow Z_{in}(\Delta w) \approx \frac{j(w_o + \Delta w)L}{-2\Delta w(w_o LC)} \approx \frac{jw_o L}{-2\Delta w(w_o LC)} = \boxed{-\frac{j}{2}\sqrt{\frac{L}{C}}\left(\frac{w_o}{\Delta w}\right)}$$

Transmission Line Version: Z(λ_0/4) with Shorted Load



- **As previously calculated**

$$\Gamma_L = \frac{Z_L - Z_o}{Z_L + Z_o} = \frac{0 - Z_o}{0 + Z_o} = -1$$

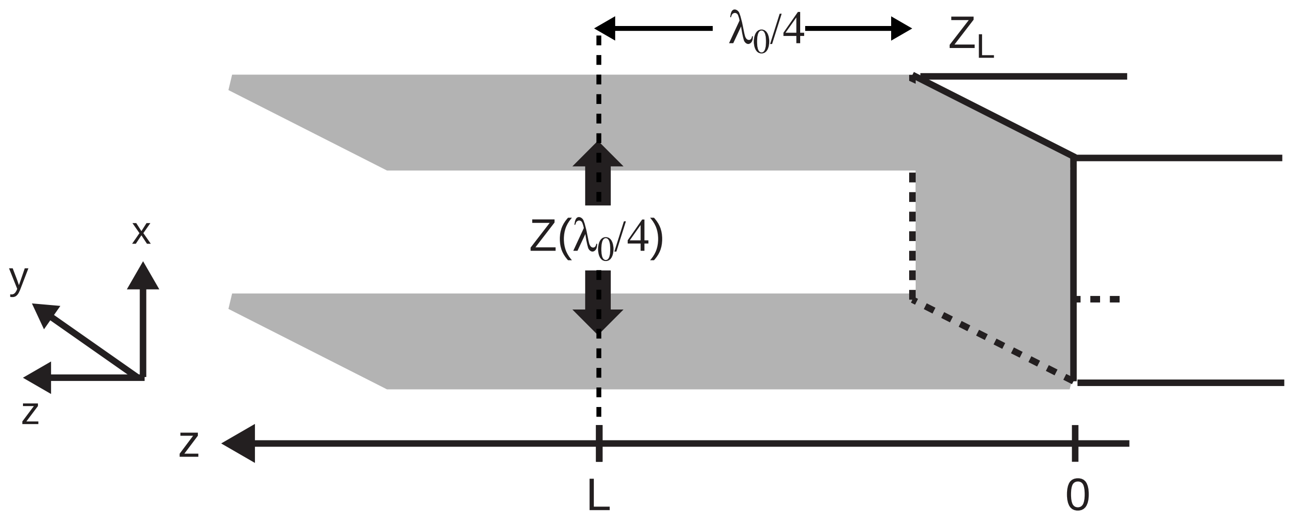
- **Impedance calculation**

$$Z(z) = Z_o \frac{1 + \Gamma(z)}{1 - \Gamma(z)}, \quad \text{where } \Gamma(z) = \Gamma_L e^{-j(4\pi/\lambda)z}$$

- **Relate λ to frequency**

$$\lambda = \frac{1}{f\sqrt{\mu\epsilon}} = \frac{1}{(f_o + \Delta f)\sqrt{\mu\epsilon}}$$

Calculate Z(Δ f) – Step 1



- **Wavelength as a function of Δ f**

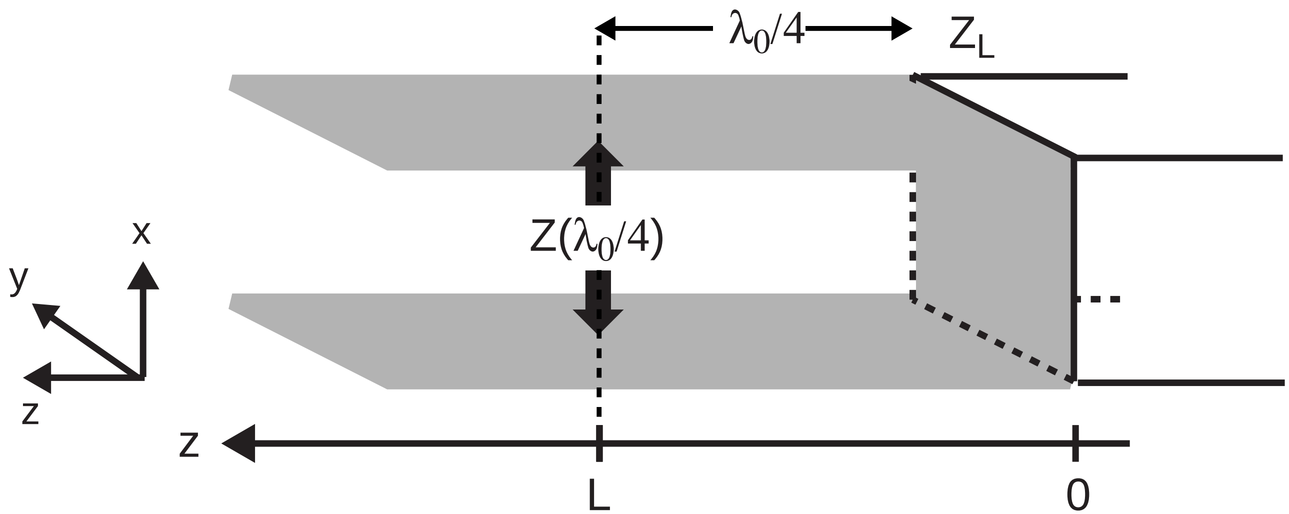
$$\lambda = \frac{1}{(f_o + \Delta f)\sqrt{\mu\epsilon}} = \frac{1}{f_o\sqrt{\mu\epsilon}(1 + \Delta f/f_o)} = \frac{\lambda_o}{1 + \Delta f/f_o}$$

- **Generalized reflection coefficient**

$$\Gamma(\lambda_o/4) = \Gamma_L e^{-j(4\pi/\lambda)\lambda_o/4} = \Gamma_L e^{-j\pi\lambda_o/\lambda} = \Gamma_L e^{-j\pi\lambda_o/\lambda}$$

$$\Rightarrow \Gamma(\lambda_o/4) = \Gamma_L e^{-j\pi(1+\Delta f/f_o)} = -\Gamma_L e^{-j\pi\Delta f/f_o}$$

Calculate Z(Δ f) – Step 2



- **Impedance calculation**

$$Z(\lambda_o/4) = Z_o \frac{1 - \Gamma_L e^{-j\pi\Delta f/f_o}}{1 + \Gamma_L e^{-j\pi\Delta f/f_o}} = Z_o \frac{1 + e^{-j\pi\Delta f/f_o}}{1 - e^{-j\pi\Delta f/f_o}}$$

- **Recall** $e^{-j\pi\Delta f/f_o} \approx 1 - j\pi\Delta f/f_o$

$$\Rightarrow \quad Z(z) \approx Z_o \frac{1 + 1 - j\pi\Delta f/f_o}{1 - 1 + j\pi\Delta f/f_o} \approx Z_o \frac{2}{j\pi\Delta f/f_o} = \boxed{-j\frac{2}{\pi}\sqrt{\frac{L}{C}}\left(\frac{w_o}{\Delta w}\right)}$$

  - **Looks like LC tank circuit (but more than one mode)!**

Smith Chart

- **Define normalized impedance**

$$Z_n = \frac{Z_L}{Z_o}$$

- **Mapping from normalized impedance to Γ is one-to-one**

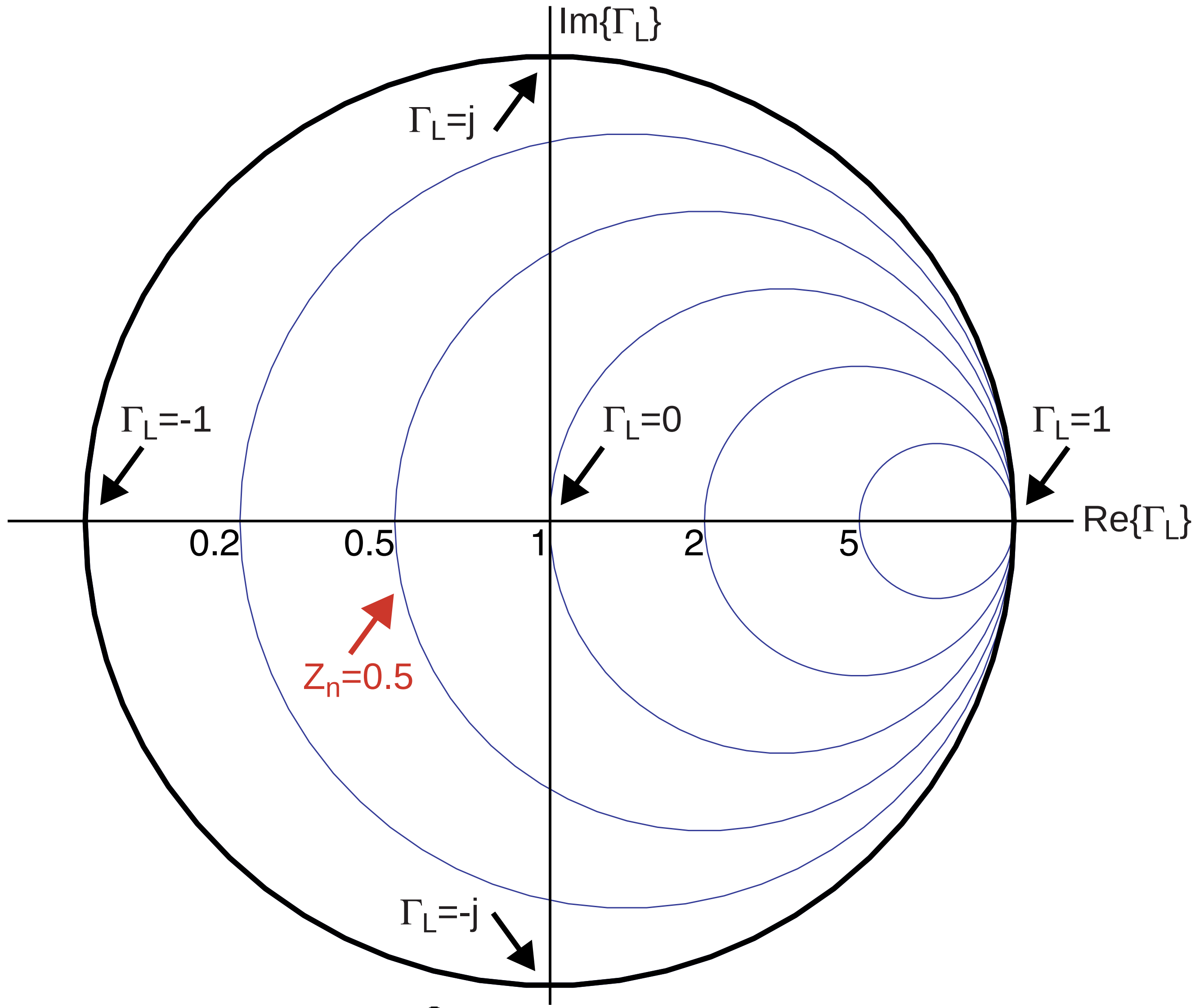
$$Z_n = \frac{1+\Gamma_L}{1-\Gamma_L}$$

  - **Consider working in coordinate system based on Γ**
- **Key relationship between Z_n and Γ**

$$Re\{Z_n\} + jIm\{Z_n\} = \frac{1 + Re\{\Gamma_L\} + jIm\{\Gamma_L\}}{1 - (Re\{\Gamma_L\} + jIm\{\Gamma_L\})}$$

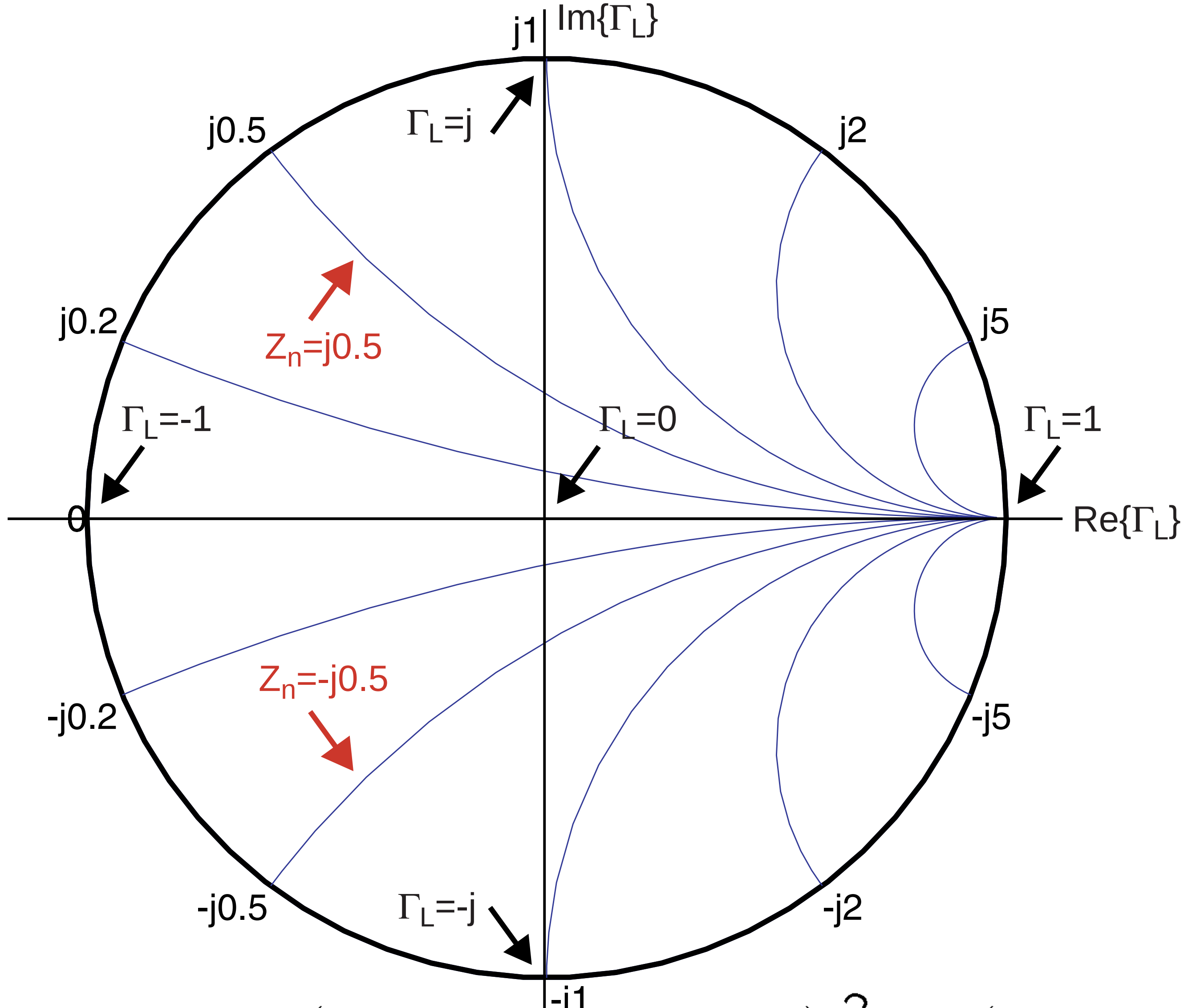
  - **Equate real and imaginary parts to get Smith Chart**

Real Impedance in Γ Coordinates (Equate Real Parts)



$$\left(Re\{\Gamma_L\} - \frac{Re\{Z_n\}}{1+Re\{Z_n\}}\right)^2 + (Im\{\Gamma_L\})^2 = \left(\frac{1}{1+Re\{Z_n\}}\right)^2$$

Imag. Impedance in Γ Coordinates (Equate Imag. Parts)



$$(Re\{\Gamma_L\} - 1)^2 + \left(Im\{\Gamma_L\} - \frac{1}{Im\{Z_n\}}\right)^2 = \left(\frac{1}{Im\{Z_n\}}\right)^2$$

What Happens When We Invert the Impedance?

- **Fundamental formulas**

$$Z_n = \frac{1+\Gamma_L}{1-\Gamma_L} \quad \Rightarrow \quad \Gamma_L = \frac{Z_n - 1}{Z_n + 1}$$

- **Impact of inverting the impedance**

$$Z_n \rightarrow 1/Z_n \quad \Rightarrow \quad \Gamma_L \rightarrow -\Gamma_L$$

  - **Derivation:**

$$\frac{1/Z_n - 1}{1/Z_n + 1} = \frac{1 - Z_n}{1 + Z_n} = -\left(\frac{Z_n - 1}{Z_n + 1}\right)$$

- **We can invert complex impedances in Γ plane by simply changing the sign of Γ !**

- **How can we best exploit this?**

The Smith Chart as a Calculator for Matching Networks

- Consider constructing both impedance and admittance curves on Smith chart

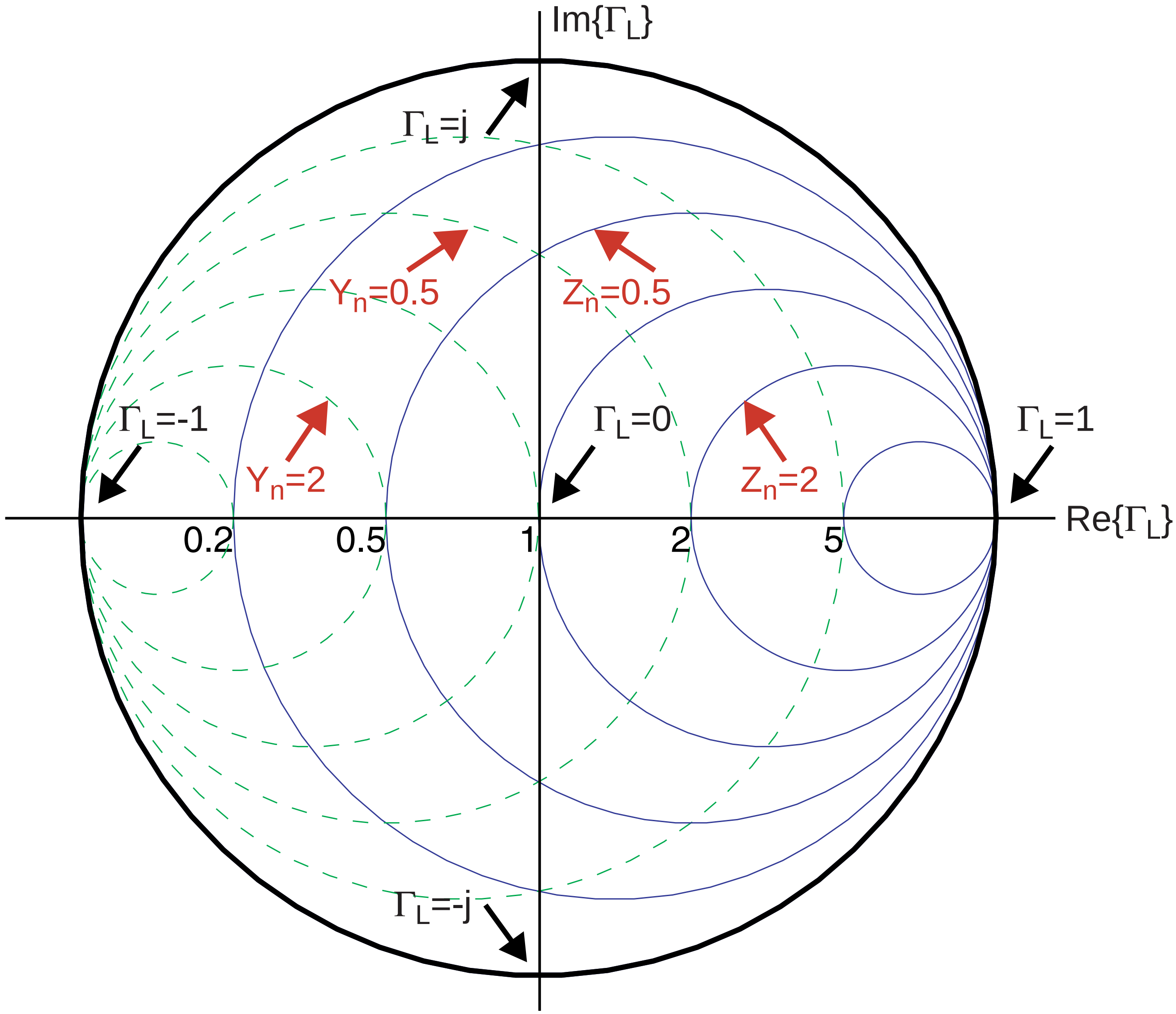
$$Z_n \rightarrow 1/Z_n \quad \Rightarrow \quad \Gamma_L \rightarrow -\Gamma_L$$

  - Conductance curves derived from resistance curves
  - Susceptance curves derived from reactance curves

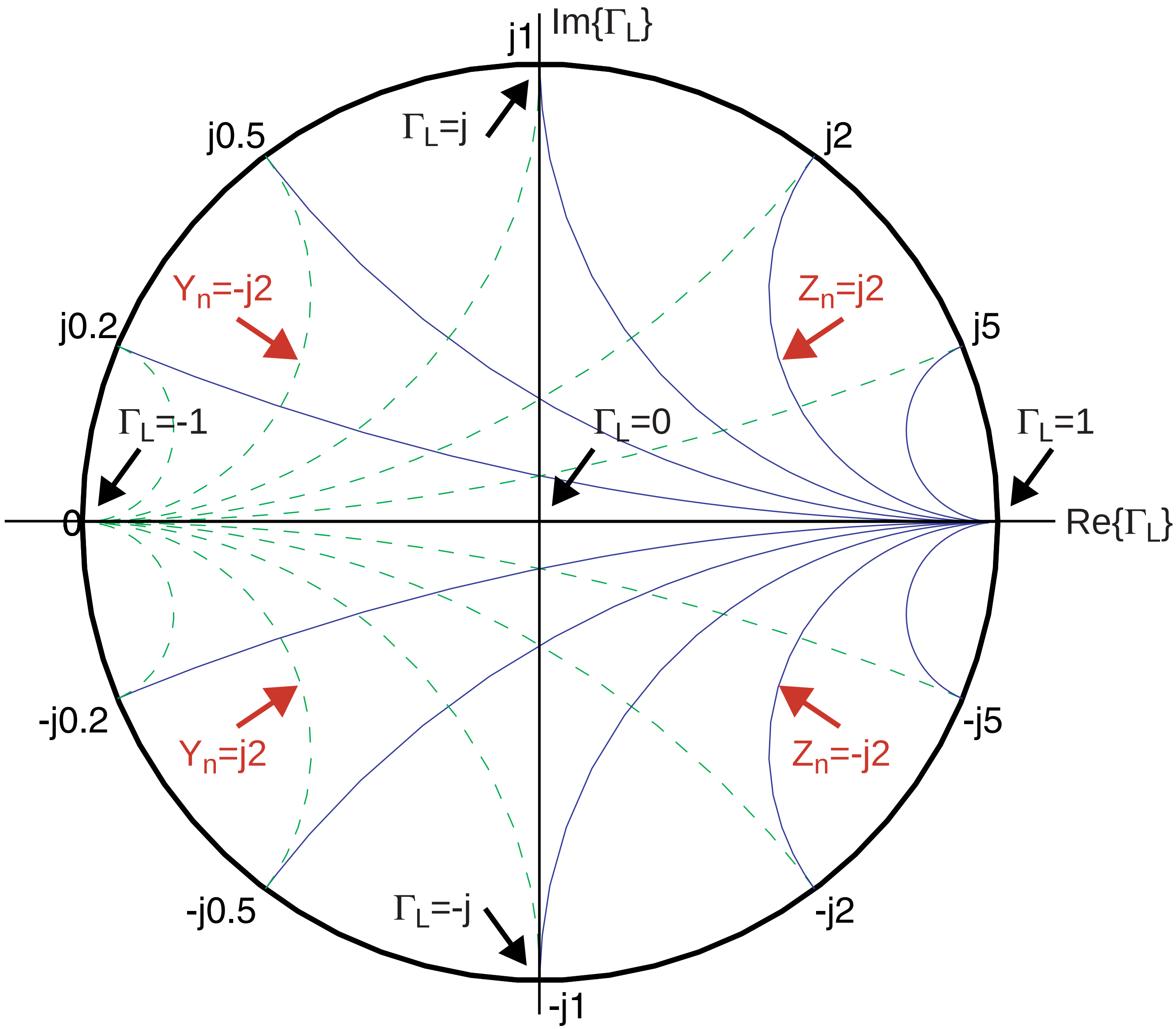
- For series circuits, work with impedance
  - Impedances add for series circuits

- For parallel circuits, work with admittance
  - Admittances add for parallel circuits

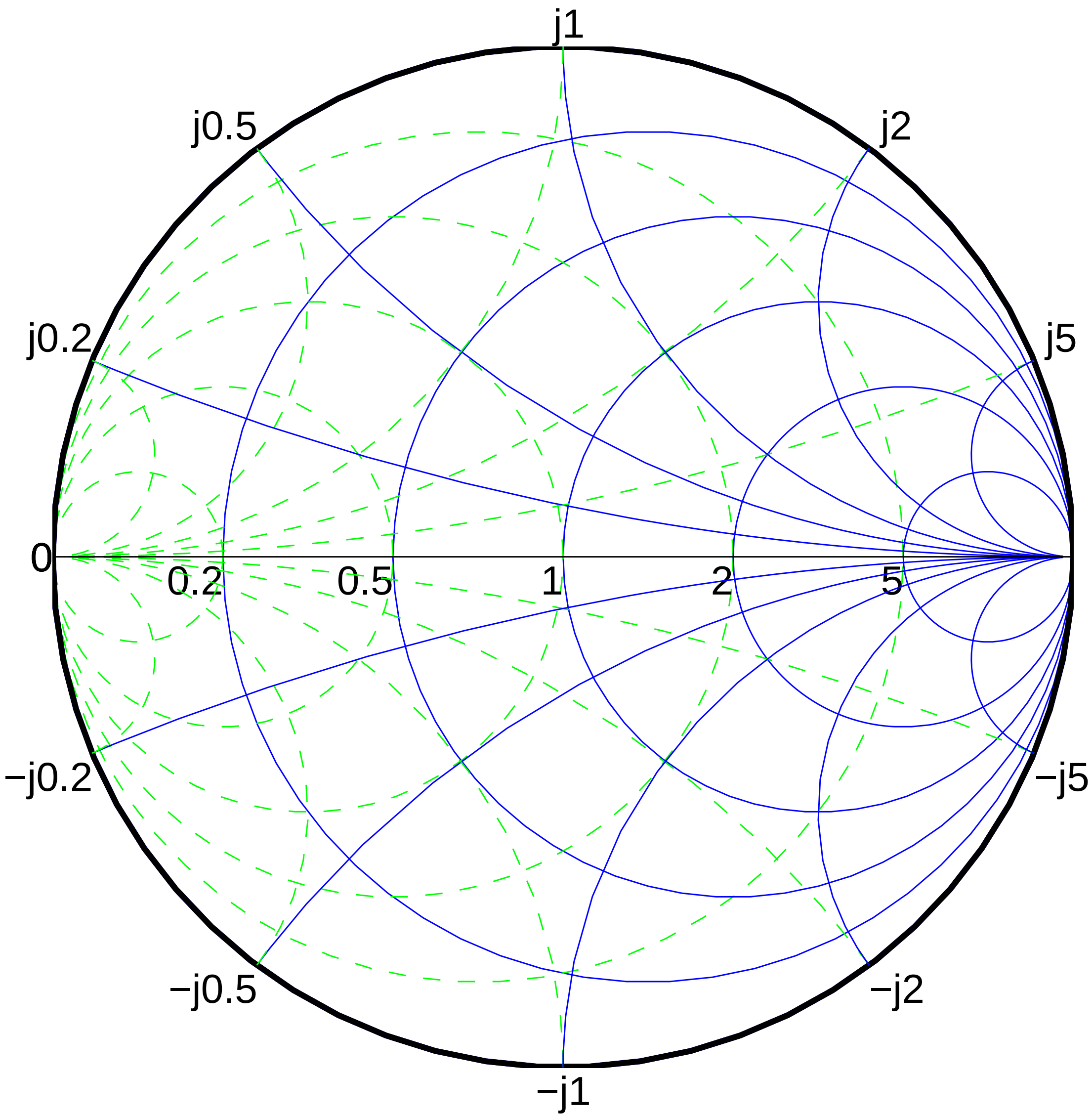
Resistance and Conductance on the Smith Chart



Reactance and Susceptance on the Smith Chart

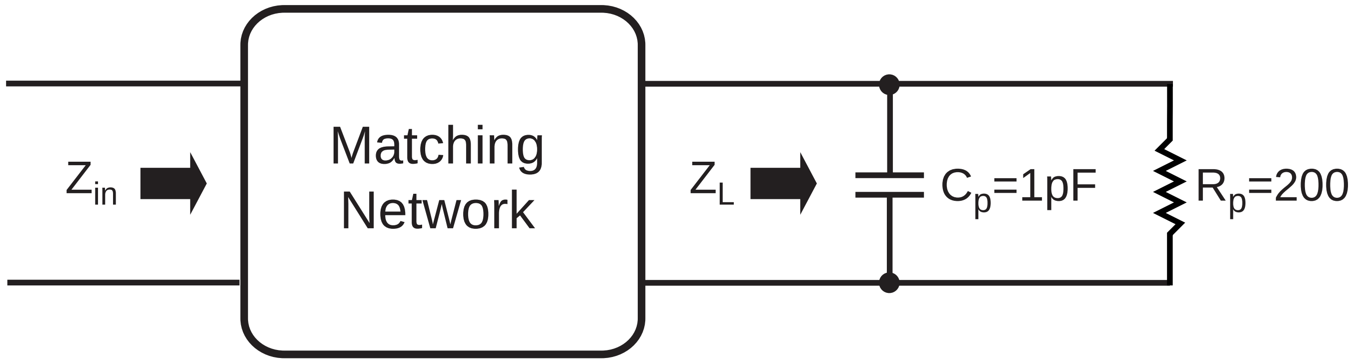


Overall Smith Chart



Example – Match RC Network to 50 Ohms at 2.5 GHz

- **Circuit**



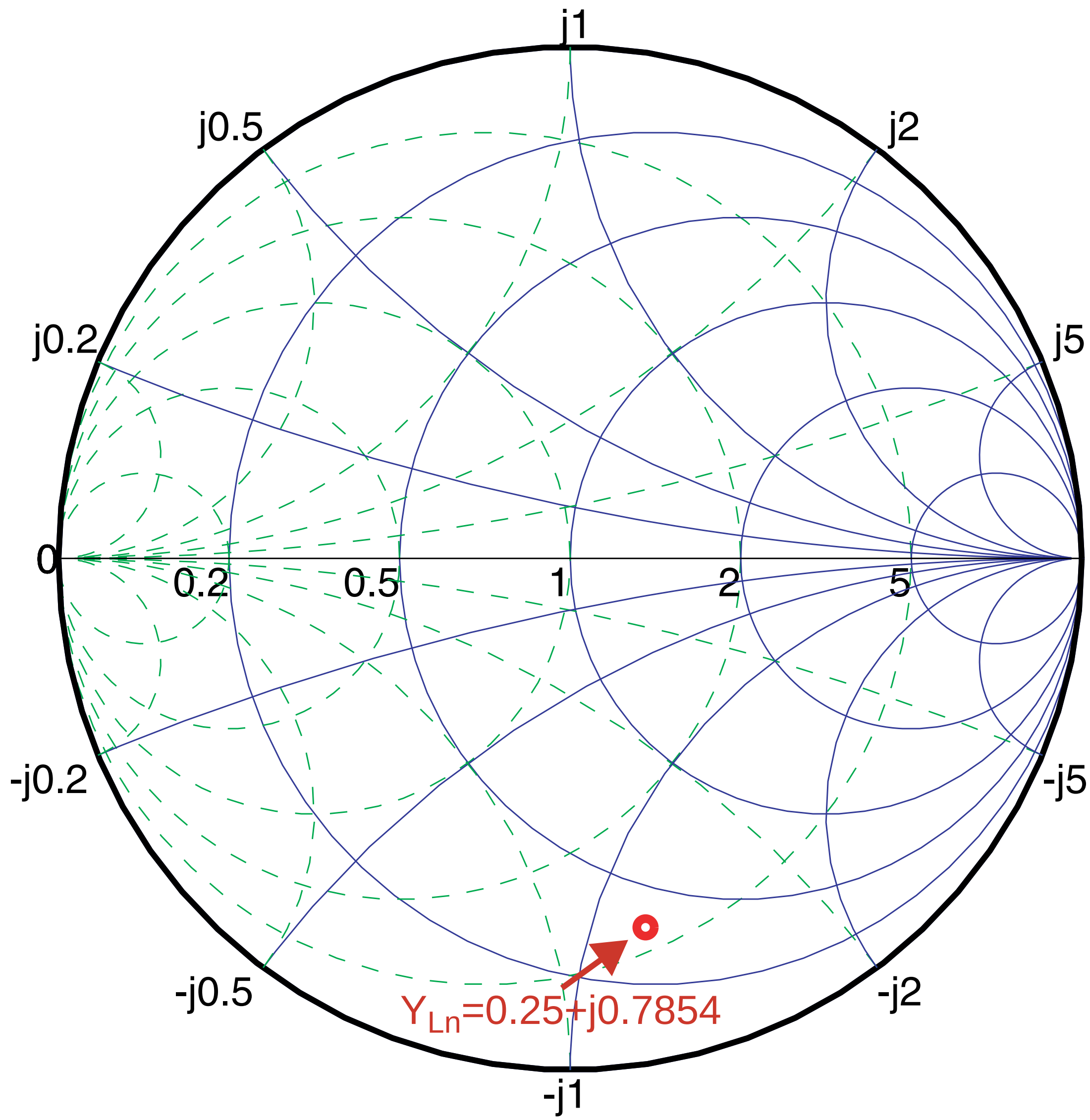
- **Step 1: Calculate Z_{Ln}**

$$Z_{Ln} = \frac{Z_L}{Z_o} = \frac{R_L||(1/jwC)}{50} = \frac{1}{50(1/R_L + jwC)}$$

$$= \frac{1}{50(1/200 + j2\pi(2.5e9)10^{-12})} = \frac{1}{0.25 + j.7854}$$

- **Step 2: Plot Z_{Ln} on Smith Chart (use admittance, Y_{Ln})**

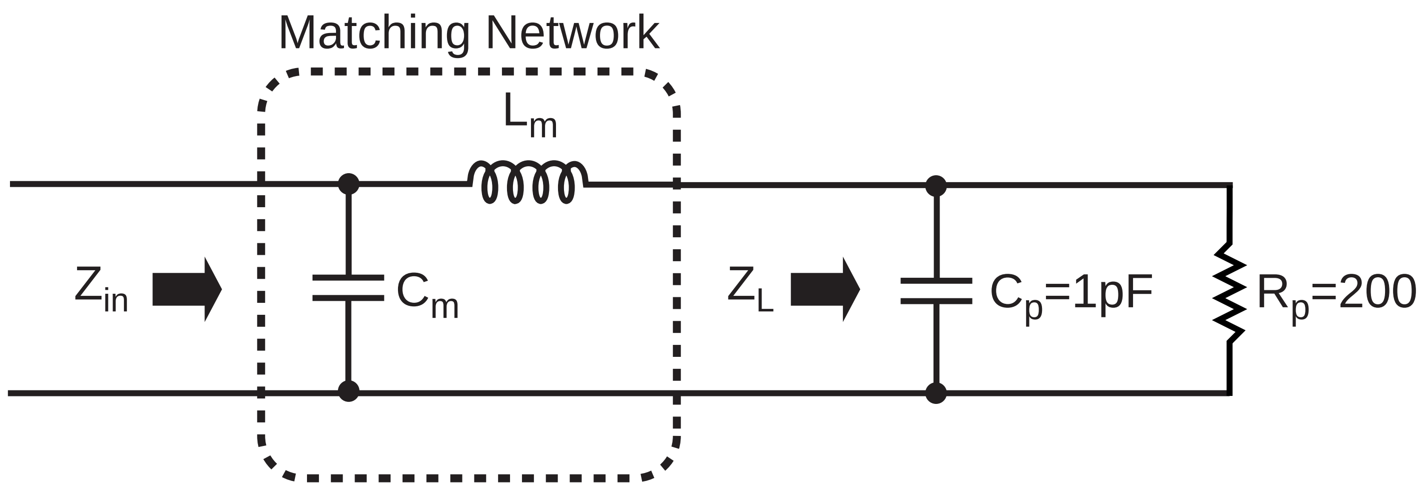
Plot Starting Impedance (Admittance) on Smith Chart



(Note: Z_{Ln}=0.37-j1.16)

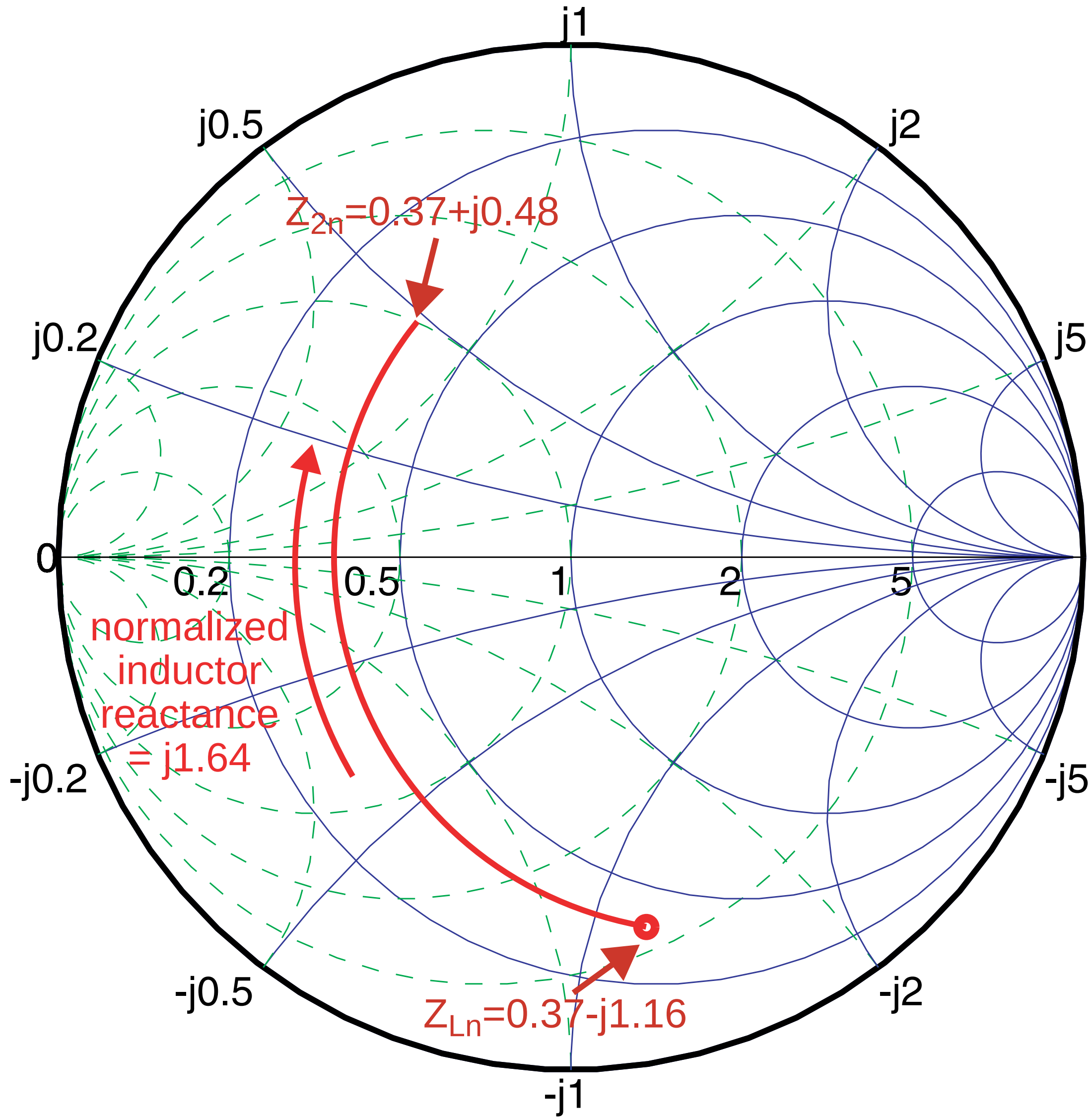
Develop Matching “Game Plan” Based on Smith Chart

- **By inspection, we see that the following matching network can bring us to Z_{in} = 50 Ohms (center of Smith chart)**



- **Use the Smith chart to come up with component values**
  - **Inductance L_m shifts impedance up along reactance curve**
  - **Capacitance C_m shifts impedance down along susceptance curve**

Add Reactance of Inductor L_m



Inductor Value Calculation Using Smith Chart

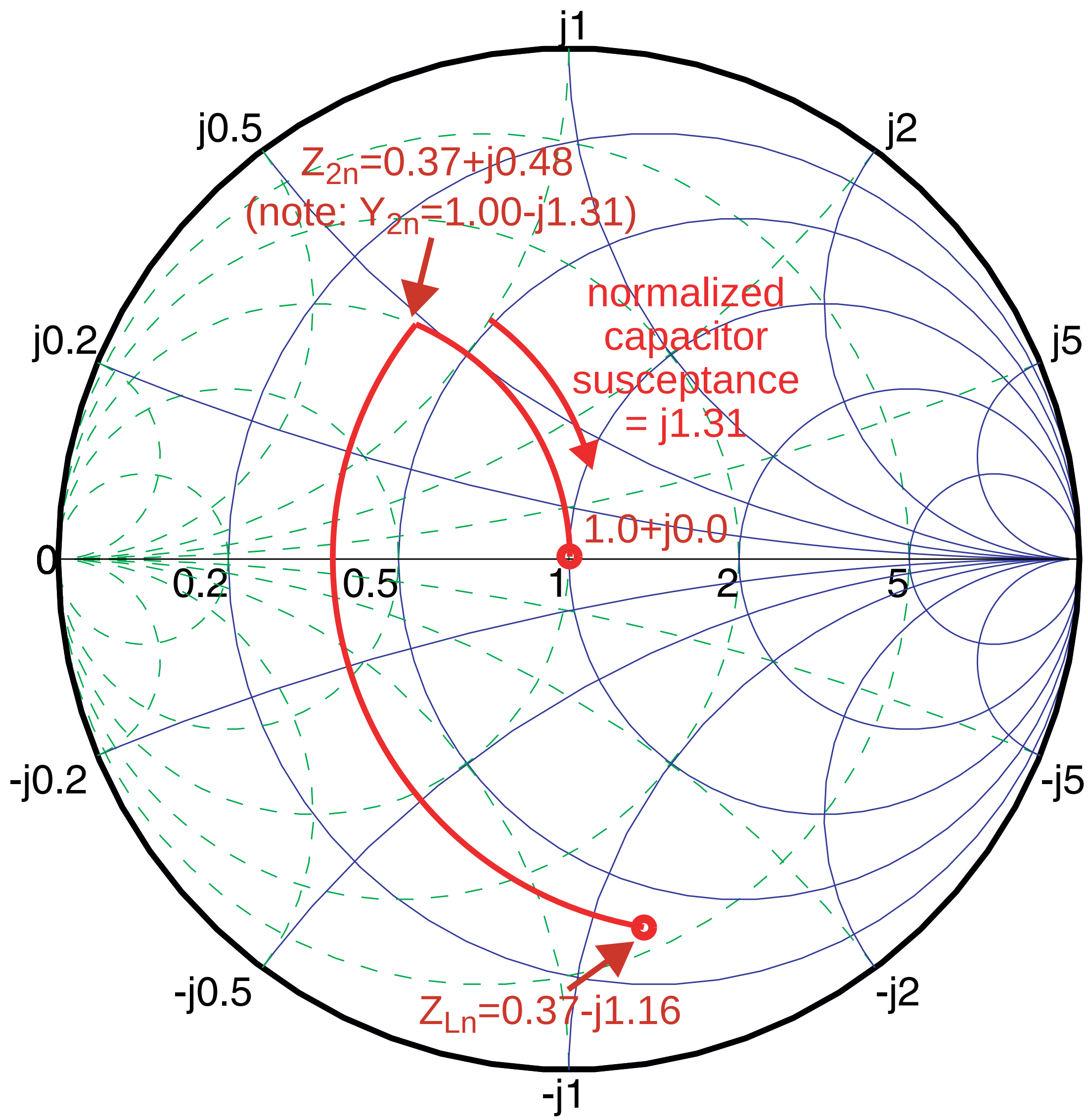
- **From Smith chart, we found that the desired normalized inductor reactance is**

$$\frac{jwL_m}{Z_o} = \frac{jwL_m}{50} = j1.64$$

- **Required inductor value is therefore**

$$\Rightarrow \quad L_m = \frac{50(1.64)}{2\pi 2.5e9} = 5.2nH$$

Add Susceptance of Capacitor C_m (Achieves Match!)



Capacitor Value Calculation Using Smith Chart

- **From Smith chart, we found that the desired normalized capacitor susceptance is**

$$Z_o jwC_m = 50jwC_m = j1.31$$

- **Required capacitor value is therefore**

$$\Rightarrow \quad C_m = \frac{1.31}{50(2\pi 2.5e9)} = 1.67pF$$

Just For Fun

- **Play the "matching game" at**

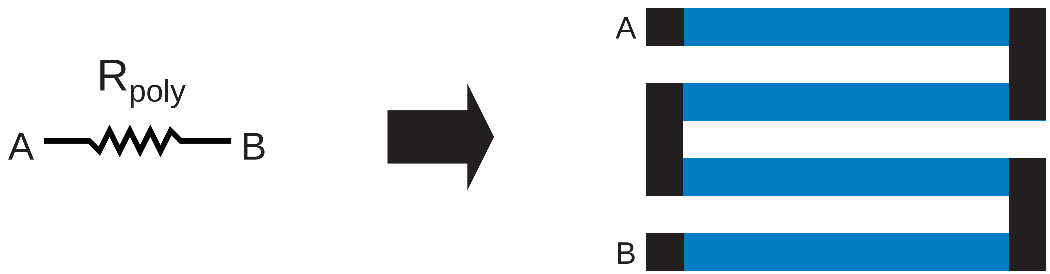
http://contact.tm.agilent.com/Agilent/tmo/an-95-1/classes/imatch.html

  - **Allows you to graphically tune several matching networks**
  - **Note: game is set up to match source to load impedance rather than match the load to the source impedance**
    - Same results, just different viewpoint

Passives

Polysilicon Resistors

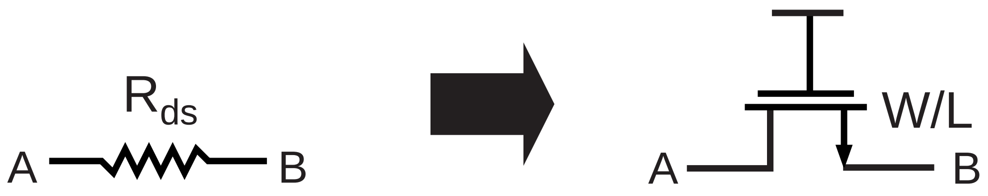
- **Use unsilicided polysilicon to create resistor**



- **Key parameters**
  - **Resistance (usually 100- 200 Ohms per square)**
  - **Parasitic capacitance (usually small)**
    - Appropriate for high speed amplifiers
  - **Linearity (quite linear compared to other options)**
  - **Accuracy (usually can be set within ± 15%)**

MOS Resistors

- Bias a MOS device in its triode region

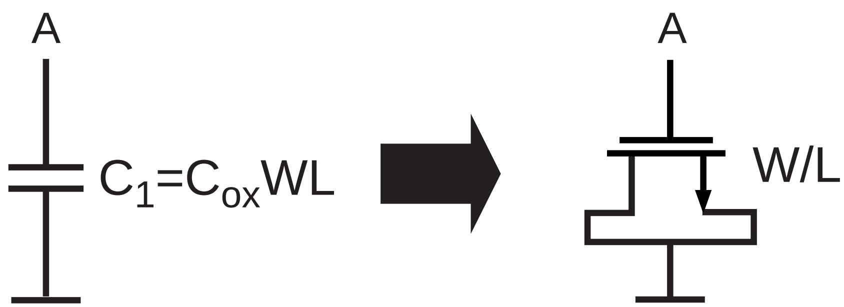


$$R_{ds} \approx \frac{1}{\mu C_{ox} W/L((V_{gs} - V_T) - V_{DS})}$$

- High resistance values can be achieved in a small area (MegaOhms within tens of square microns)
- Resistance is quite nonlinear
  - Appropriate for small swing circuits

High Density Capacitors (Biasing, Decoupling)

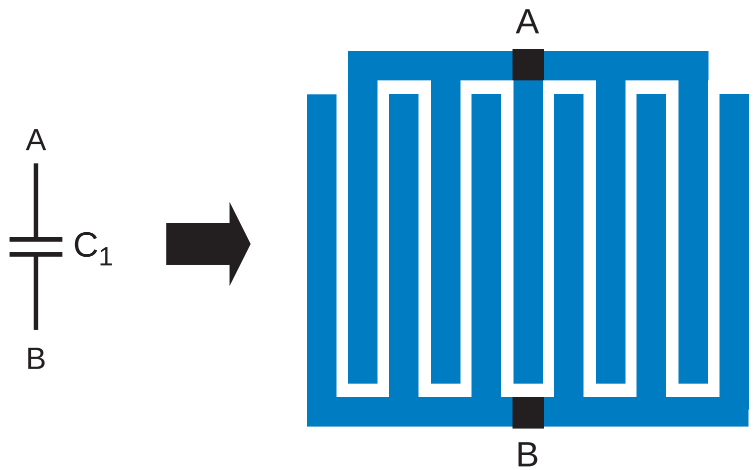
- **MOS devices offer the highest capacitance per unit area**
  - **Limited to a one terminal device**
  - **Voltage must be high enough to invert the channel**



- **Key parameters**
  - **Capacitance value**
    - Raw cap value from MOS device is 6.1 fF/μ m^2 for 0.24u CMOS
  - **Q (i.e., amount of series resistance)**
    - Maximized with minimum L (tradeoff with area efficiency)
- **See pages 39-40 of Tom Lee's book**

High Q Capacitors (Signal Path)

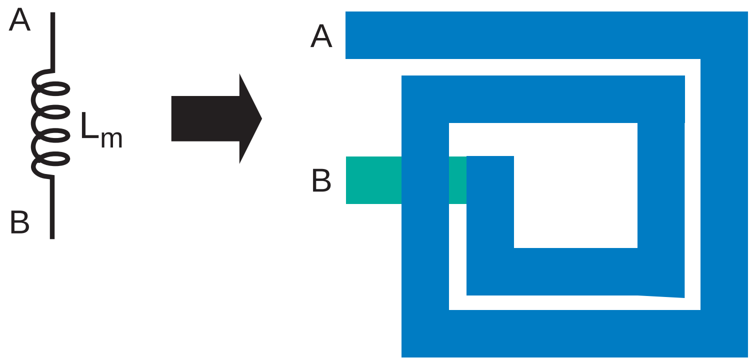
- **Lateral metal capacitors offer high Q and reasonably large capacitance per unit area**
  - **Stack many levels of metal on top of each other (best layers are the top ones), via them at maximum density**



  - **Accuracy often better than $\pm$10%**
  - **Parasitic side cap is symmetric, less than 10% of cap value**
- **Example: C_T = 1.5 fF/μm^2 for 0.24μm process with 7 metals, L_{min} = W_{min} = 0.24μm, t_{metal} = 0.53μm**
  - see “Capacity Limits and Matching Properties of Integrated Capacitors”, Aparicio et. al., JSSC, Mar 2002

Spiral Inductors

- **Create integrated inductor using spiral shape on top level metals (may also want a patterned ground shield)**

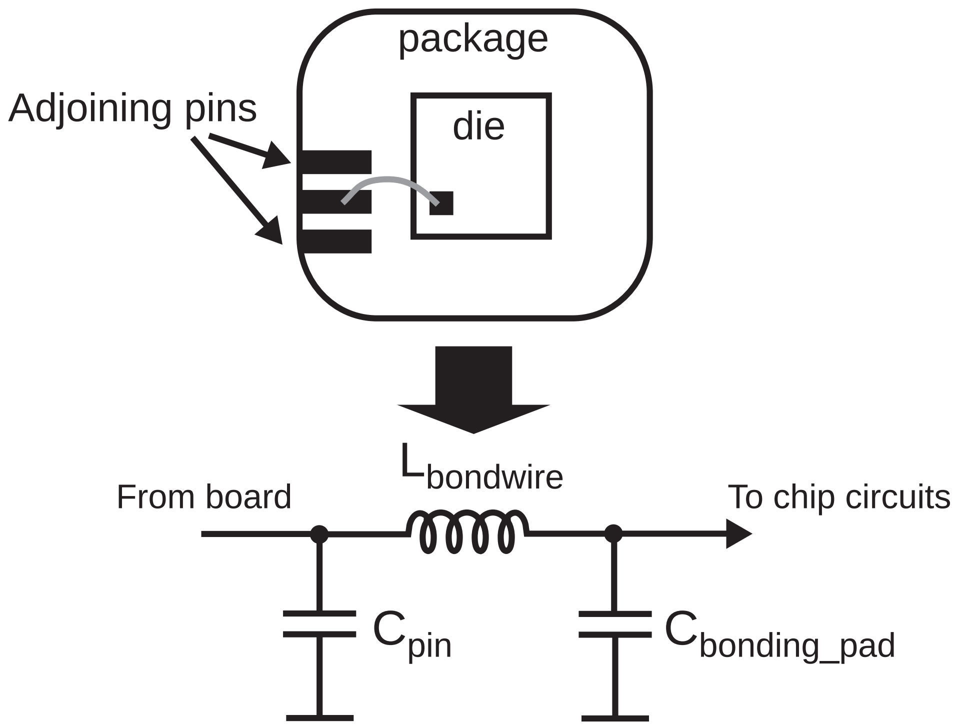


  - **Key parameters are Q (< 10), L (1-10 nH), self resonant freq.**
  - **Usually implemented in top metal layers to minimize series resistance, coupling to substrate**
  - **Design using Mohan et. al, "Simple, Accurate Expressions for Planar Spiral Inductances, JSSC, Oct, 1999, pp 1419-1424**
  - **Verify inductor parameters (L, Q, etc.) using ASITIC**

    http://formosa.eecs.berkeley.edu/~niknejad/asitic.html

Bondwire Inductors

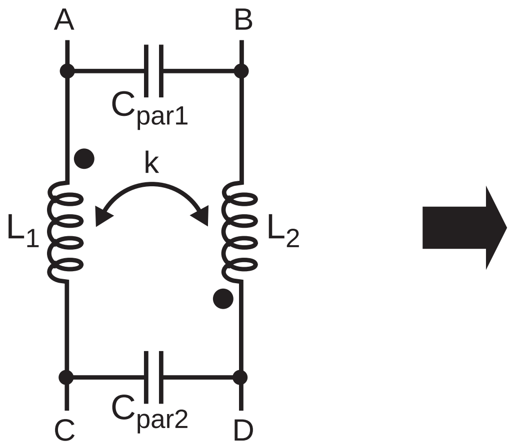
- **Used to bond from the package to die**
  - **Can be used to advantage**

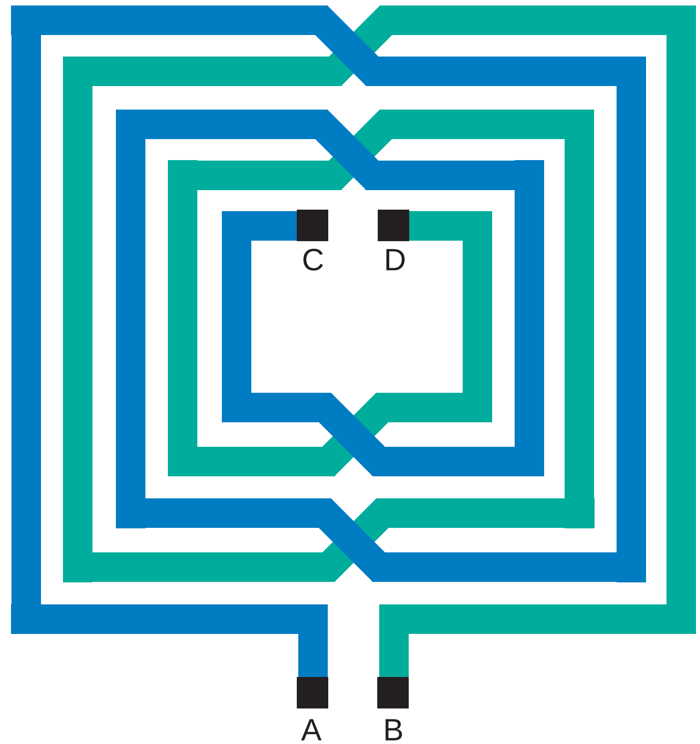


- **Key parameters**
  - **Inductance (≈ 1 nH/mm – usually achieve 1-5 nH)**
  - **Q (much higher than spiral inductors – typically > 40)**

Integrated Transformers

- **Utilize magnetic coupling between adjoining wires**





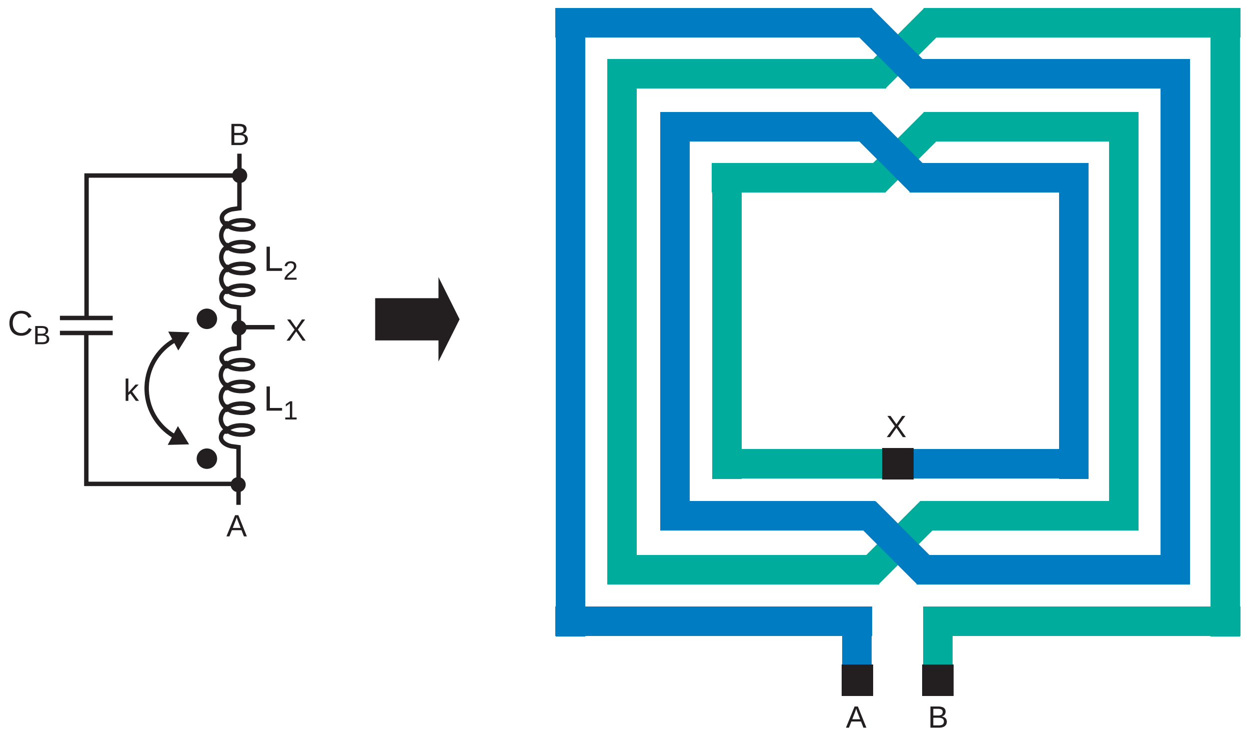
- **Key parameters**
  - **L (self inductance for primary and secondary windings)**
  - **k (coupling coefficient between primary and secondary)**

Note: $k = \dfrac{M}{\sqrt{L_1 L_2}}$ where M = mutual inductance

- **Design – ASITIC, other CAD packages**

High Speed Transformer Example – A T-Coil Network

- **A T-coil consists of a center-tapped inductor with mutual coupling between each inductor half**



- **Used for bandwidth enhancement**
  - **See S. Galal, B. Ravazi, "10 Gb/s Limiting Amplifier and Laser/Modulator Driver in 0.18u CMOS", ISSCC 2003, pp 188-189 and "Broadband ESD Protection …", pp. 182-183**