

Analysis and Design of Analog Integrated Circuits
Lecture 2

Two-Port Models, Frequency Response

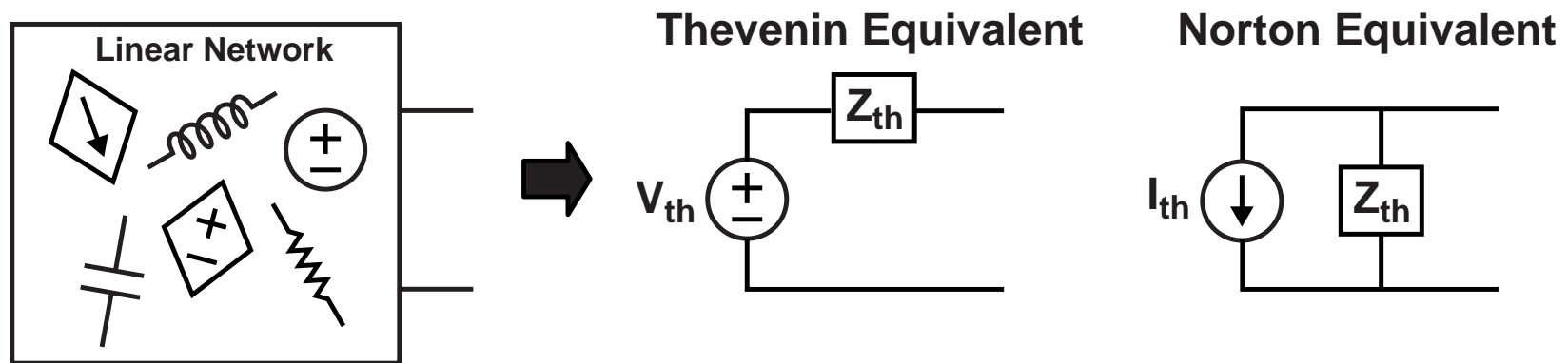
Michael H. Perrott

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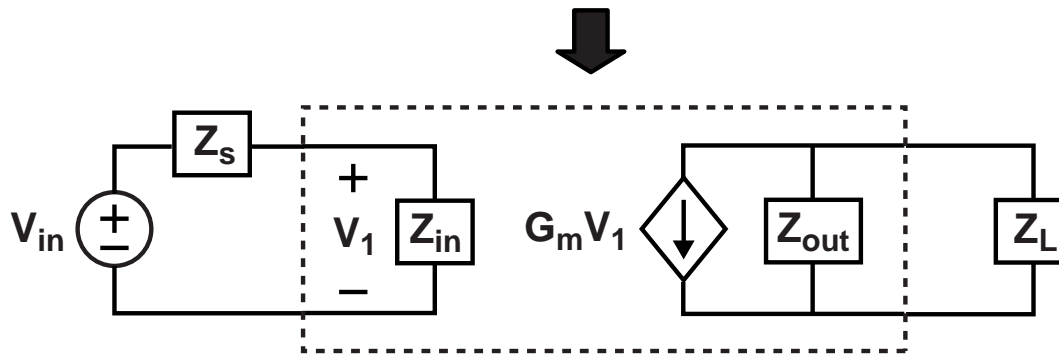
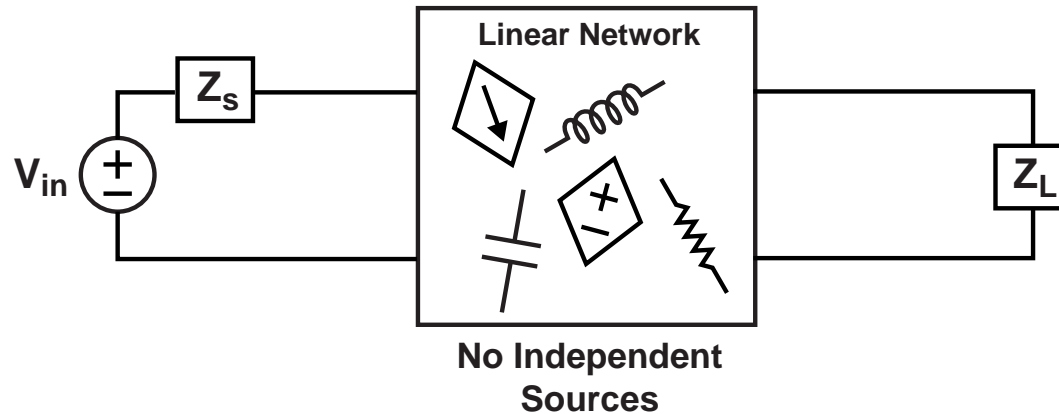
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Review: Basics of One-Port Modeling

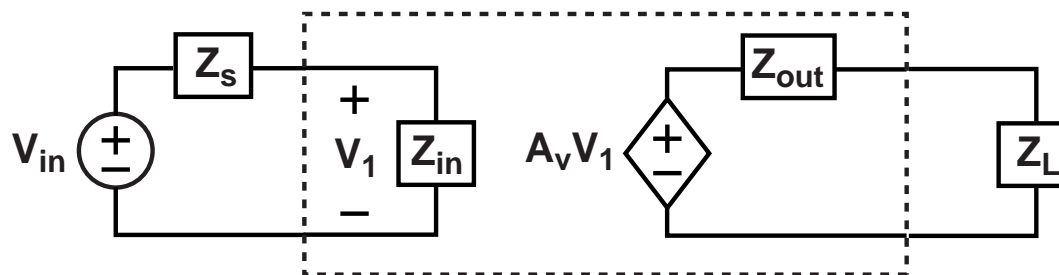


- V_{th} computed as open circuit voltage at port nodes
- I_{th} computed as short circuit current across port nodes
- Z_{th} computed as V_{th}/I_{th}
 - All independent voltage and current sources are set to zero value

Basics of Two-Port Modeling (Unilateral)

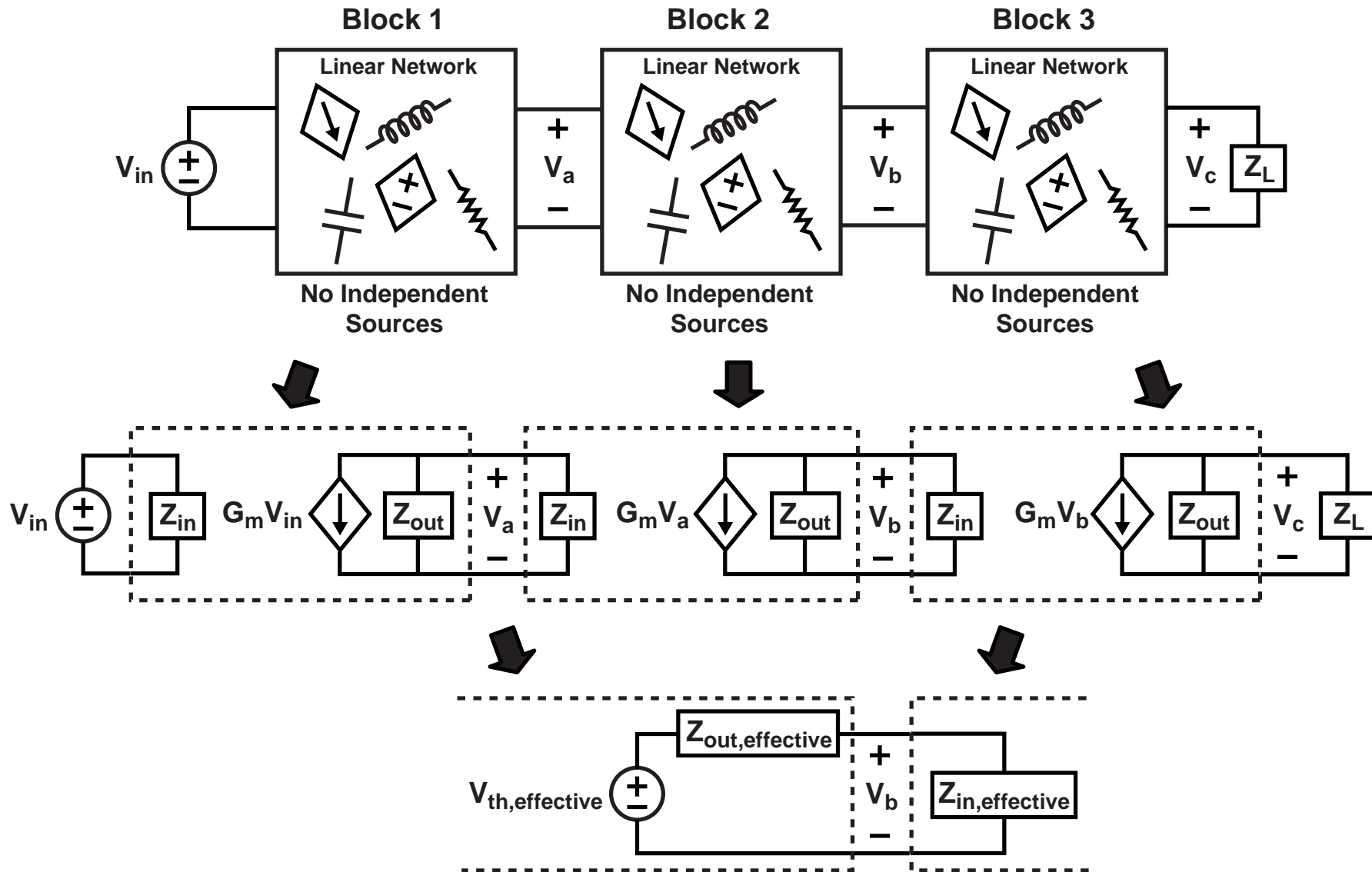


OR



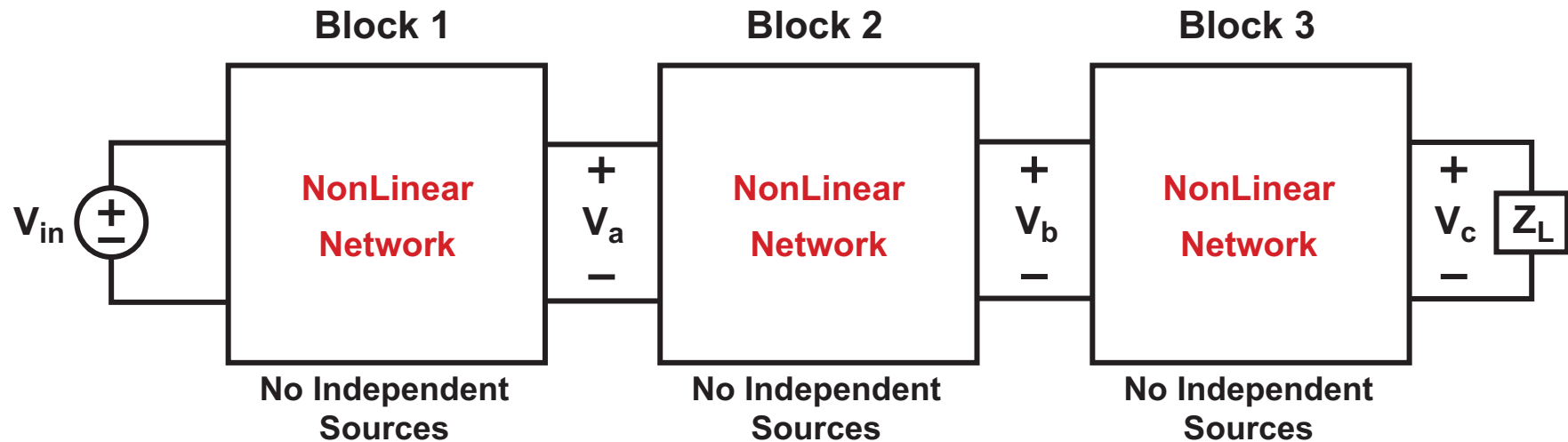
- We now include a dependent current or voltage source
- Z_{in}
 - Solve using 1-Port analysis at input
- Z_{out}
 - Solve using 1-Port analysis at output with $V_1 = 0$
- G_M
 - Short circuit output current as a function of V_1
- A_v
 - Open circuit output voltage as a function of V_1

Analysis of Cascaded Blocks



Analysis carried out without solving simultaneous equations!

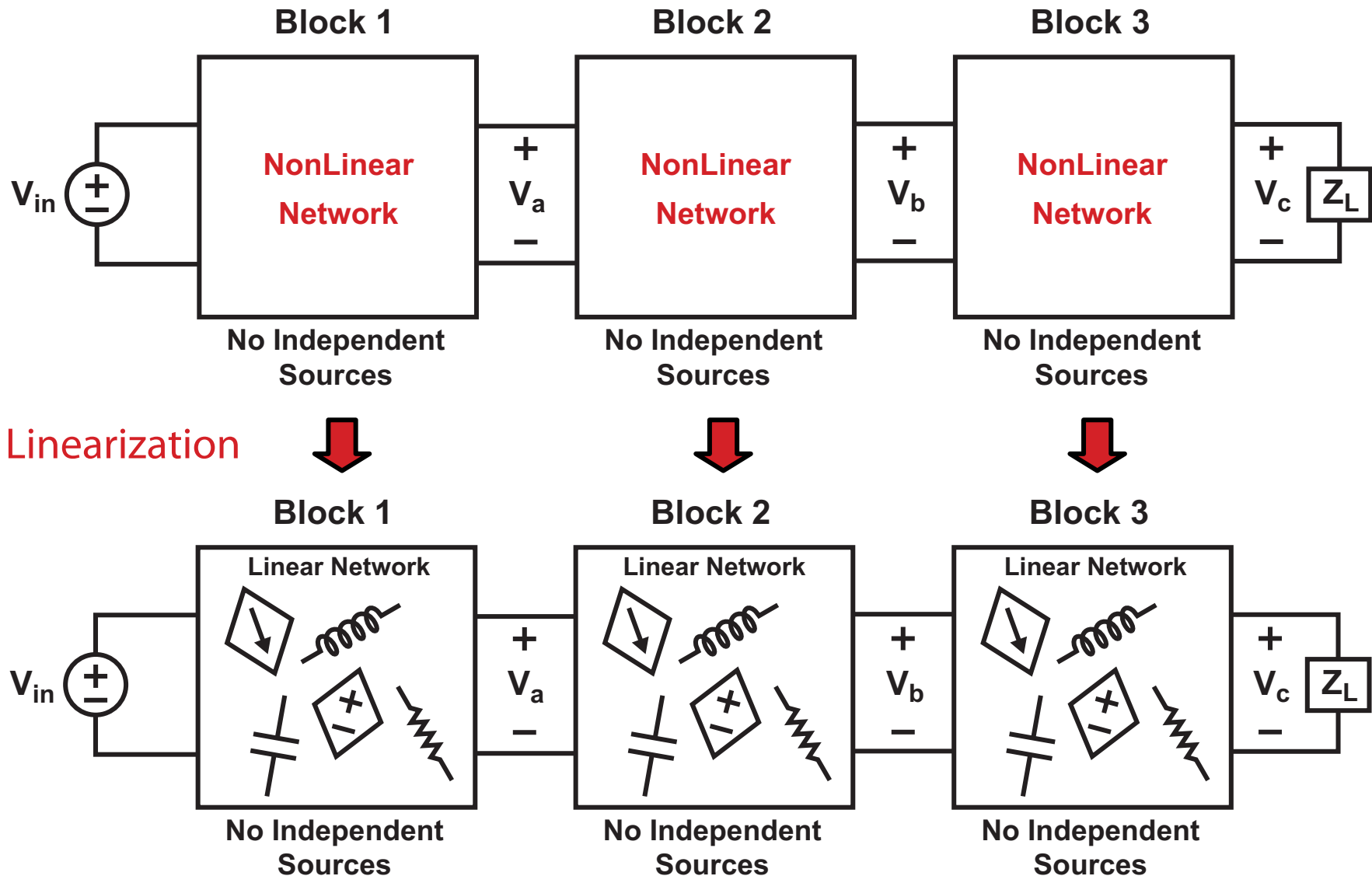
Problem: Most Circuits are Very Nonlinear!



- Thevenin/Norton modeling only applies to linear networks
- Direct analysis of nonlinear networks is challenging

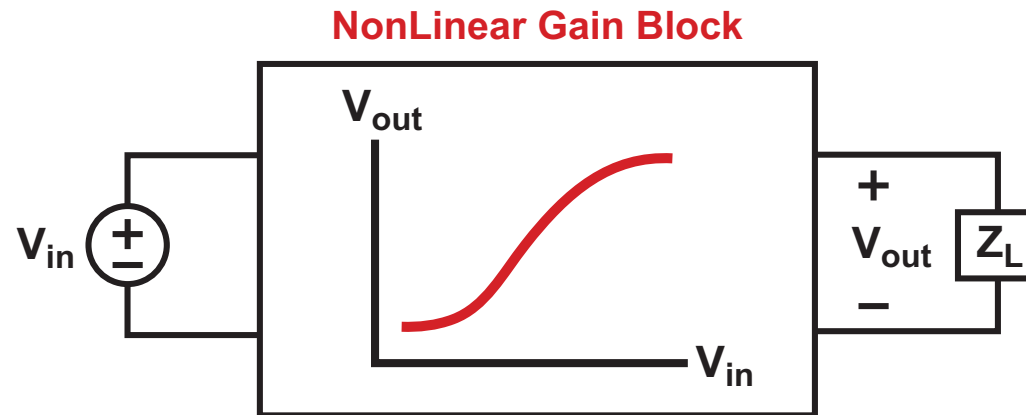
Can we still leverage two-port modeling?

Small Signal Modeling Allows Us to Linearize



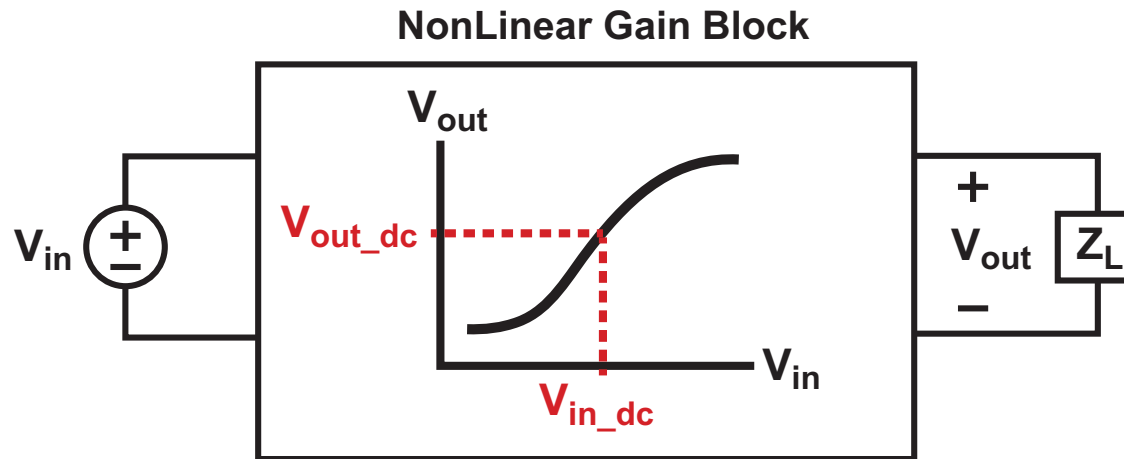
Small signal model is only valid about a specific operating point

Small Versus Large Signal Modeling



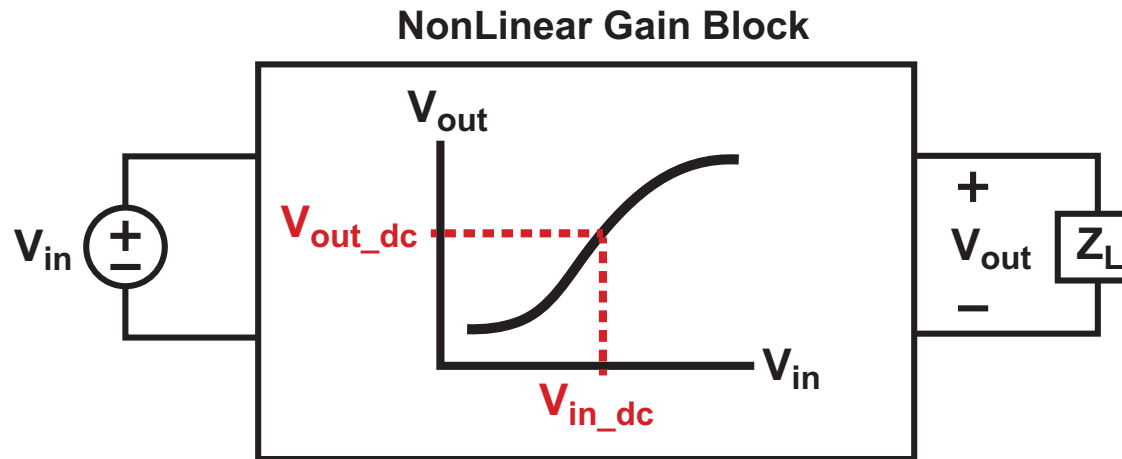
- Sketch V_{out} versus V_{in} as the amplitude of V_{in} is increased

Impact of Operating Point on Small Signal Modeling



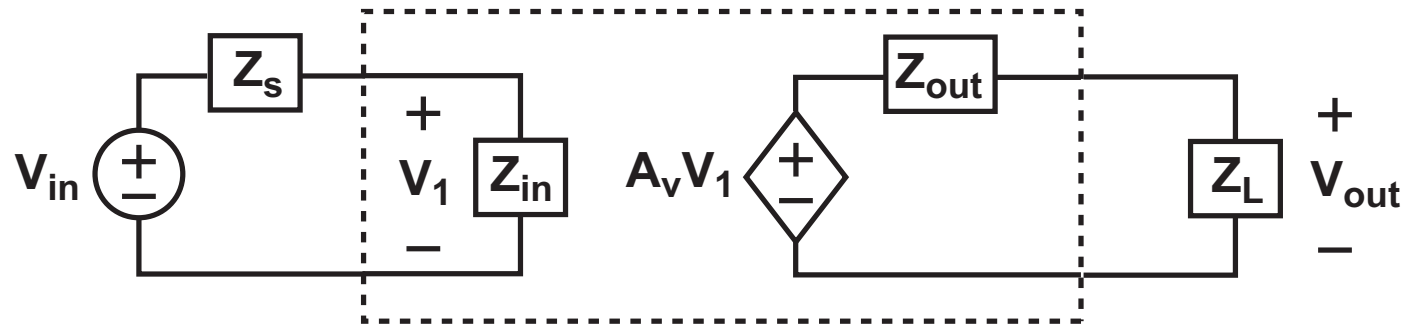
- Sketch V_{out} versus V_{in} as the DC operating point is changed

Achieving a Small Signal Model



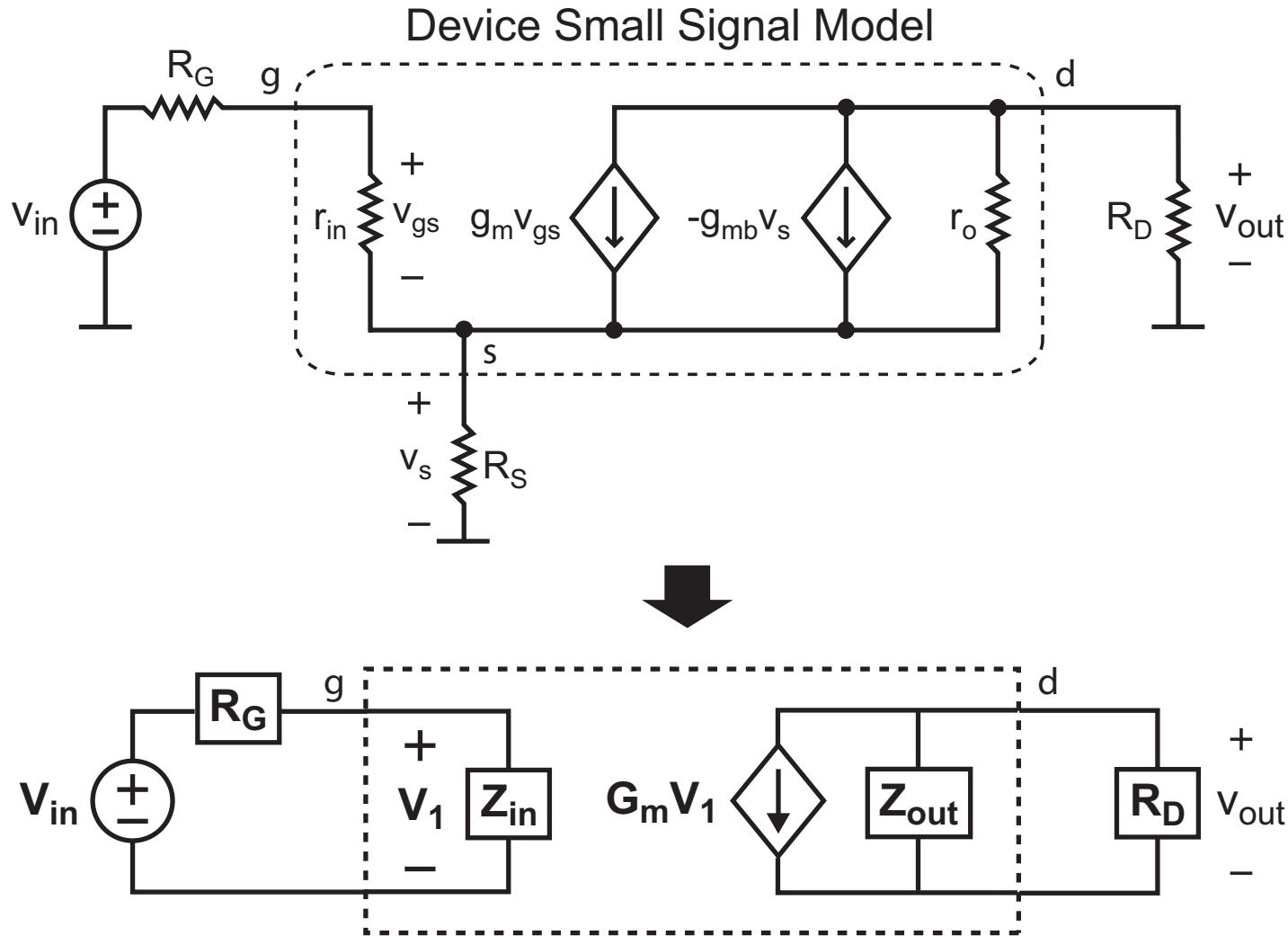
- Create a two port model of the above block

Including Impedances in Two-Port Models



- Compute V_{out} as a function of V_{in}

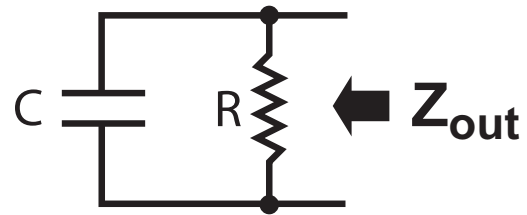
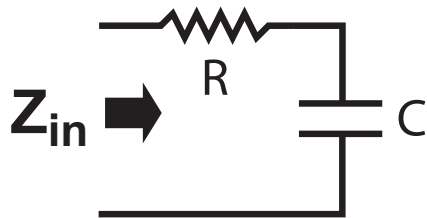
Example of Two-Port Derivation



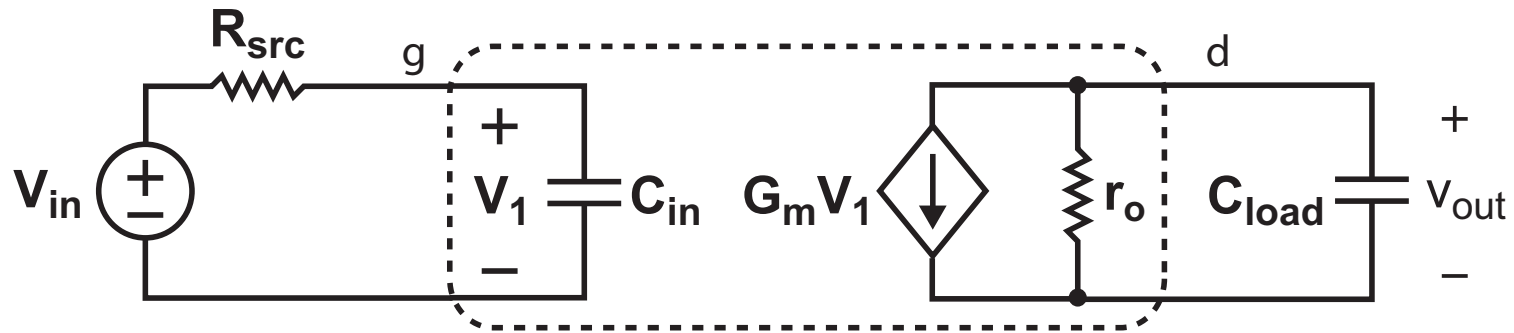
- Compute Z_{in} , Z_{out} , and G_m
 - Assume $r_{in} = \text{infinity}$, $g_{mb} = 0$

Frequency Domain Modeling of Impedances

- Determine Laplace Transform of Impedances Below:



Example: Transfer Function of Two-Port Circuit



- Derive the transfer function $V_{out}(s)/V_{in}(s)$
- Label the poles and zeros of the transfer function

Frequency Response

- Frequency response is readily derived from a transfer function:
 - For w (rad/s), you substitute $s = jw$
 - For f (Hz), you substitute $s = j2\pi f$
 - Note that $j = \text{sqrt}(-1)$
- Example, for the transfer function on the previous page, the frequency response (in f (Hz)) is:

Bode Plot Basics

- The magnitude and phase of the frequency response is often depicted in the form of a Bode plot

- **Example:**
$$H(w) = \frac{V_{out}(w)}{V_{in}(w)} = \frac{1 + jw/w_z}{(1 + jw/w_{p1})(1 + jw/w_{p2})}$$

- **Log of magnitude (dB):** $20 \log |H(w)|$

$$= 20 \log |1 + jw/w_z| - 20 \log |1 + jw/w_{p1}| - 20 \log |1 + jw/w_{p2}|$$

- Taking the log allows the poles and zeros to be plotted separately and then added together

- **Phase:** $\angle H(w)$

$$= \angle(1 + jw/w_z) - \angle(1 + jw/w_{p1}) - \angle(1 + jw/w_{p2})$$

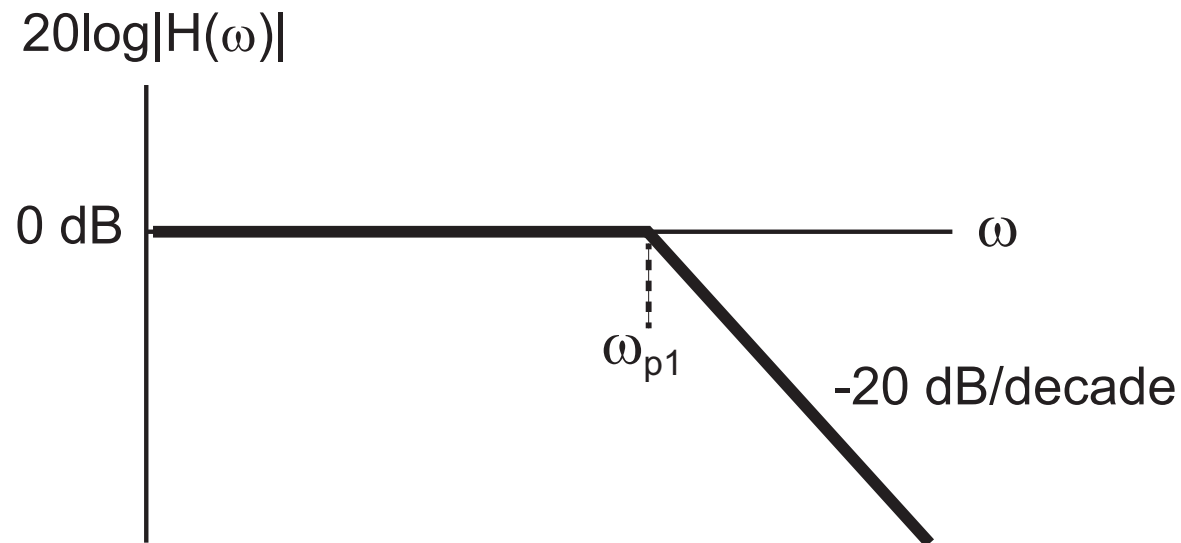
- Phase of poles and zeros can also be plotted separately and then added together

Plotting the Magnitude of Poles

- Plot the magnitude response of pole w_{p1}

$$20 \log |H(w)| = 20 \log \left| \frac{1}{1 + jw/w_{p1}} \right| = -20 \log |1 + jw/w_{p1}|$$

- For $w \ll w_{p1}$: $20 \log |H(w)| \approx -20 \log |1| = 0$
- For $w \gg w_{p1}$: $20 \log |H(w)| \approx -20 \log |w/w_{p1}|$

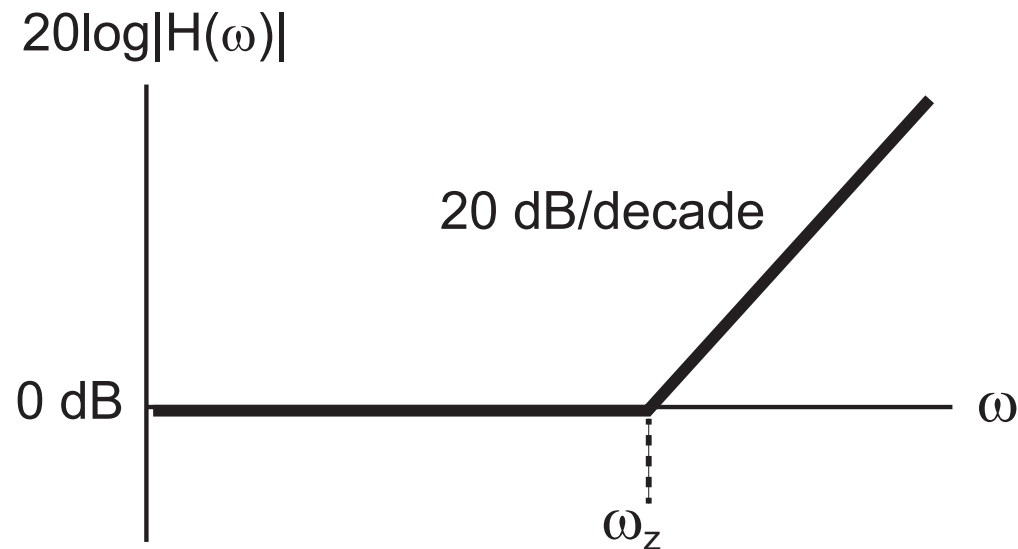


Plotting the Magnitude of Zeros

- Plot the magnitude response of pole w_z

$$20 \log |H(w)| = 20 \log |1 + jw/w_z|$$

- For $w \ll w_z$: $20 \log |H(w)| \approx 20 \log |1| = 0$
- For $w \gg w_z$: $20 \log |H(w)| \approx 20 \log |w/w_z|$

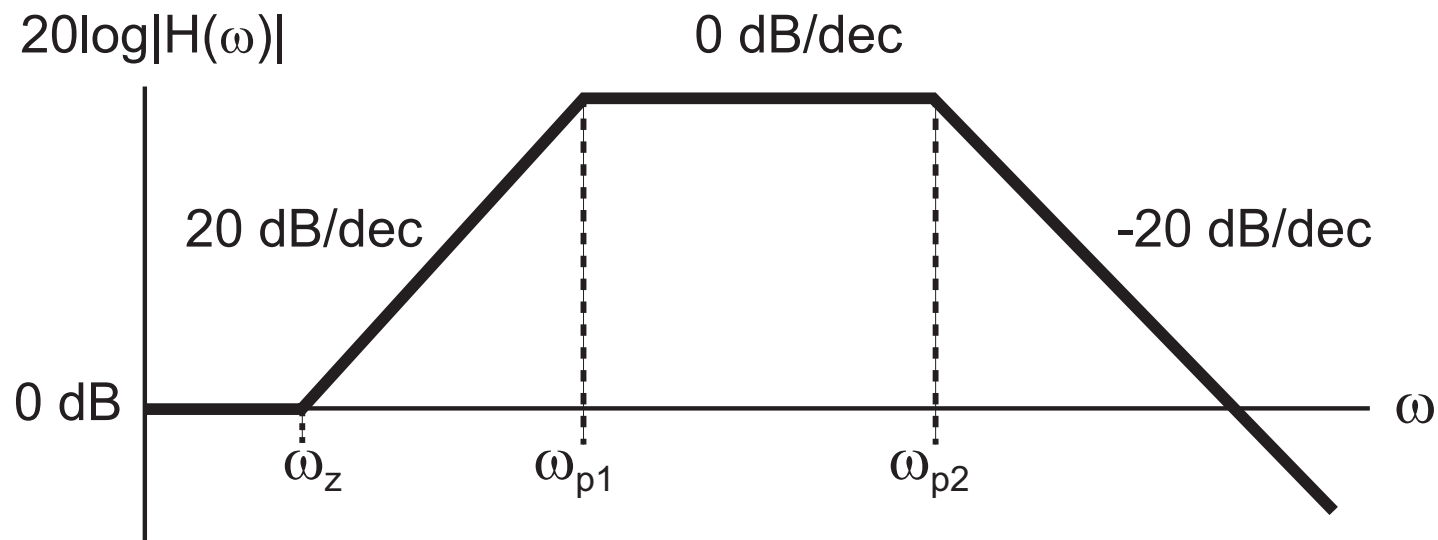


Putting It All Together

■ Example Frequency Response:

$$H(\omega) = \frac{V_{out}(\omega)}{V_{in}(\omega)} = \frac{1 + j\omega/\omega_z}{(1 + j\omega/\omega_{p1})(1 + j\omega/\omega_{p2})}$$

- Assume $\omega_z \ll \omega_{p1} \ll \omega_{p2}$



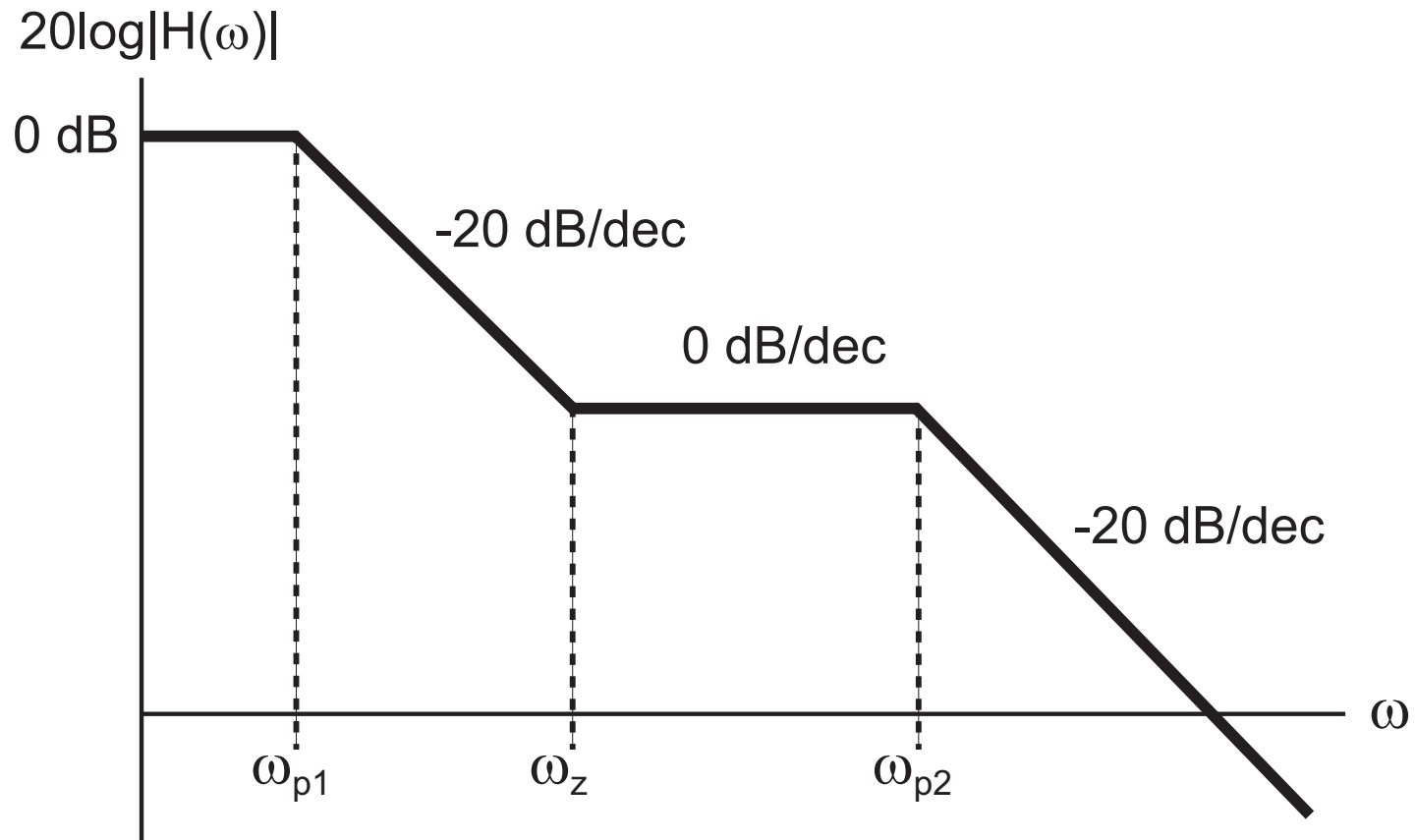
- What happens if $\omega_{p1} \ll \omega_z \ll \omega_{p2}$?

Changing the Order of Poles and Zeros

■ Example Frequency Response:

$$H(\omega) = \frac{V_{out}(\omega)}{V_{in}(\omega)} = \frac{1 + j\omega/\omega_z}{(1 + j\omega/\omega_{p1})(1 + j\omega/\omega_{p2})}$$

- Assume $\omega_{p1} \ll \omega_z \ll \omega_{p2}$



Changing the DC Gain from 1 to K

■ Example Frequency Response:

$$H(w) = \frac{V_{out}(w)}{V_{in}(w)} = K \frac{1 + jw/w_z}{(1 + jw/w_{p1})(1 + jw/w_{p2})}$$

- Assume $w_{p1} \ll w_z \ll w_{p2}$

